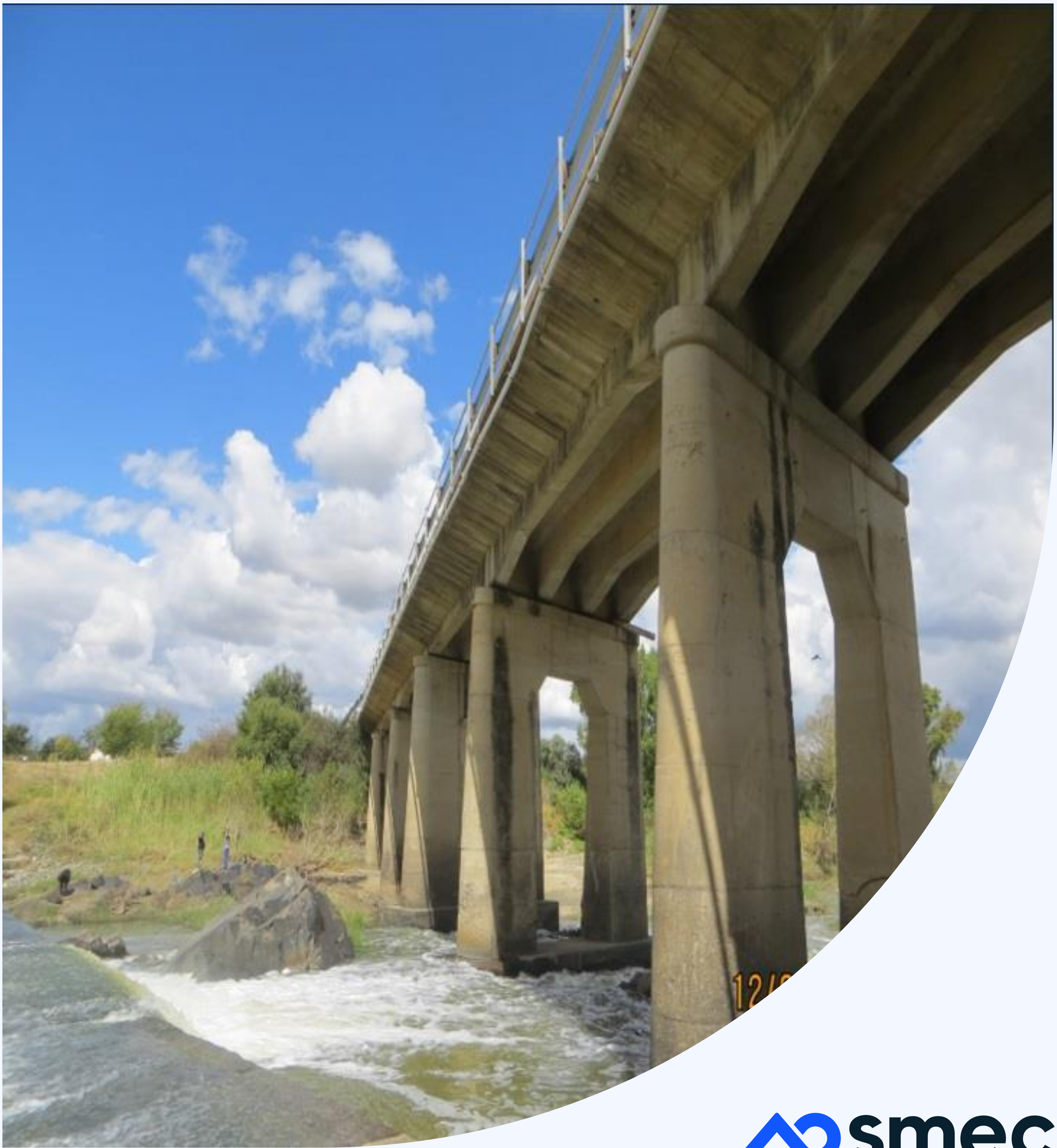
Design Report

Tetra4 Gas Hydrological Assessment

Prepared for: EIMS (Pty) Ltd
16 May 2025
Client Reference No. 1743



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SMEC Company Details

Approved by	Nicholas Franz
Address	267 Kent Avenue, Ferndale, Randburg, 2194
Phone	011 369 0600
Email	nicholas.franz@smec.com
Website	www.smec.com
Signature	

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Address: Tel: Email:	Name	
	Role	
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Address: Tel: Email:	Name	
	Role	
	Date	
Approved by Consultant(s)	SMEC South Africa (Pty) Ltd	
Approval (01)	Signature	
Address: Tel: Email:	Name	Nicholas Franz
	Role	Project Manager
	Date	2025-05-16
Approval (02)	Signature	
Address: Tel: Email:	Name	Neil Meyer
	Role	Technical Principal
	Date	2025-05-16

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I, Rendani Thovhakale, Neil Meyer and Johan Badenhorst, representing SMEC South Africa (PTY) Ltd., hereby declare that I am an independent consultant appointed to provide specialist input for the hydrological component of an Environmental Impact Assessment (EIA) study for the proposed Gas Cluster 2 project. I confirm that I have no personal financial interest other than the remuneration of the EIA study itself, neither I nor SMEC South Africa (Pty) Ltd will benefit in any other away from the outcomes of the Gas Cluster 2 project. I further declare that opinions expressed in this report have been formulated in an objective manner without interference from any third party.

Name	Signature	Date
Rendani Thovhakale		27-July-2022
Neil Meyer		27-July-2022
Johan Badenhorst		24-January-2025

Authors

Summary of Expertise:

Rendani Thovhakale

Rendani is a registered ECSA Candidate Civil Engineer with 6 years of experience in undertaking Hydrological impact assessments. He has specialist skills in hydrological analysis and hydraulic modelling. Rendani has worked on similar hydrological projects based in 6 different countries including Lesotho, Mauritius, South Africa, Eswatini, Guinea and Mali. He has undertaken Environmental Impact Assessment (EIA) studies in the hydrology specialist area with adherence to relevant legislation and guidelines including the National Water Act, Act 36 of 1998 (NWA) aimed at the protection of water resources.

Neil Meyer

Neil is a registered ECSA Professional Civil Engineer with 23 years of experience in the design and project management of various projects both in South Africa and internationally, plus design and project management of bulk and municipal water, sanitation and drainage infrastructure including water and wastewater treatment projects. He has completed his MSc. Eng at the University of Stellenbosch from 2000 to 2001 and his MSc. Eng HEM/DIC at the University of London, United Kingdom from 2001 to 2002.

Johan Badenhorst

Johan is registered with ECSA as a Professional Engineering Technologist with 38 years of experience in construction supervision, and design of projects involving water conveyance and drainage in South Africa, Lesotho, and Saudi Arabia. His skills include topographical modelling, field investigations, hydrological analysis, hydraulic modelling and design of drainage structure.

Contents

Figures

Tables

Abbreviations and Acronyms

Abbreviation / Acronym / Symbol	Explanation / Description
EIA	Environmental Impact Assessment
EA	Environmental Authorisation
EMPr	Environmental Management Programme
km^2	Square kilometres
m	Meters
m^3/s	Cubic meters per second
m/s	Meters per second
Ml	Megalitres
SWMP	Storm Water Management Plan
WUL	Water Use Licence

1. Introduction

SMEC South Africa (Pty) Ltd. was appointed by EIMS to undertake a Hydrological Study for the proposed Tetra4 Gas Cluster 2 located in the Free State, South Africa. Tetra4 (Pty) Ltd aims to extend its natural gas operations inside the project area indicated in Figure 1-1.

The purpose of this hydrological study is to serve as a component of the Environmental Impact Assessment (EIA) study. The objectives of this EIA phase are to determine the overall impacts and potential mitigation measures, on the hydrological environment, in order to ensure environmental legal compliance and efficient, cost-effective surface water management.

The project area is situated approximately 10 kilometres (km) south of Welkom, as shown in Figure 1-1 below. The approximate geographical coordinates of the centre of project area are:

- Latitude - 28°10'00"S
- Longitude - 26°44'00"E

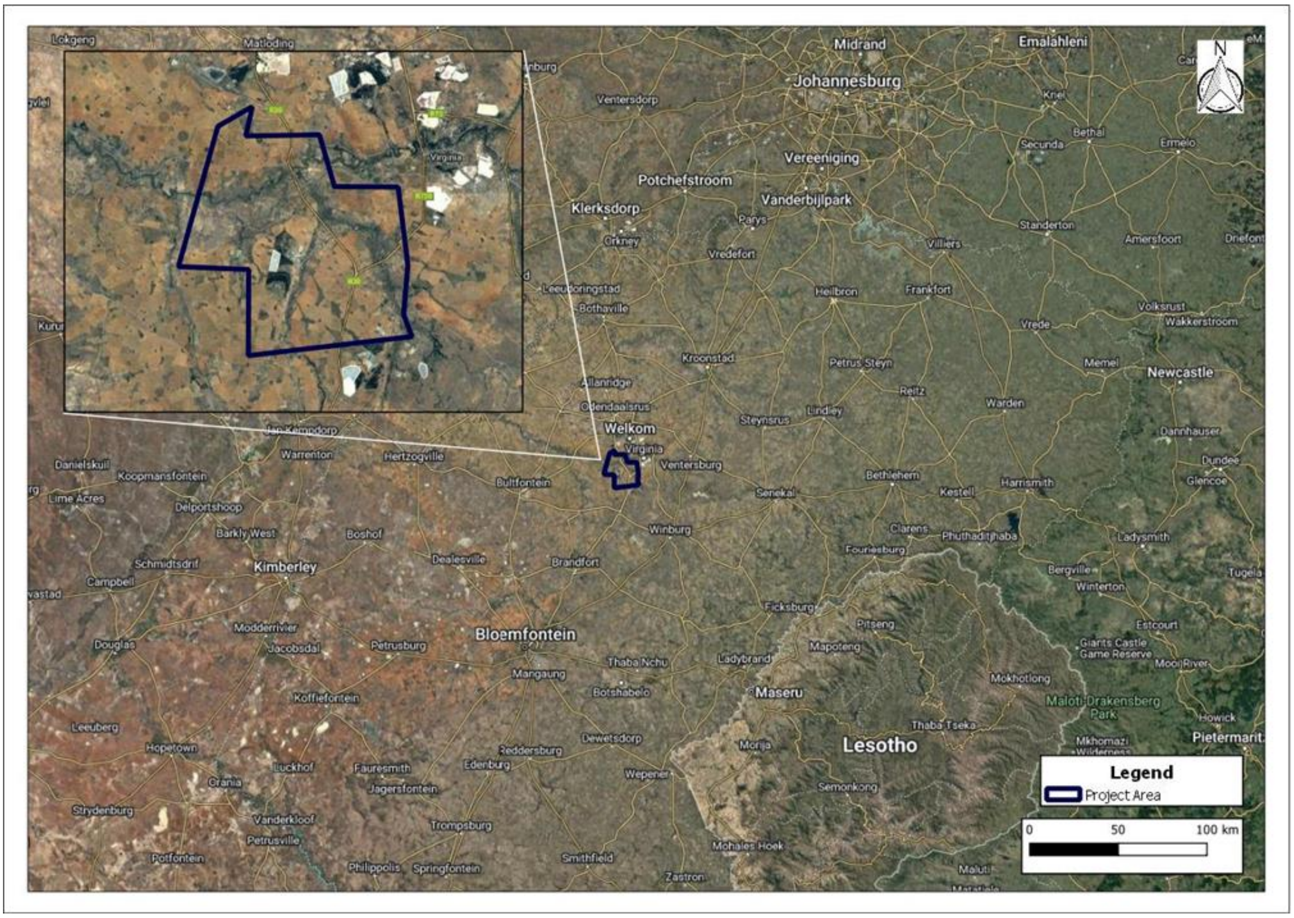

Figure 1-1: Project Area Location

The extent of the Project area boundary is shown in Figure 1-2. The area of the site is approximately 27 500 Hectares.

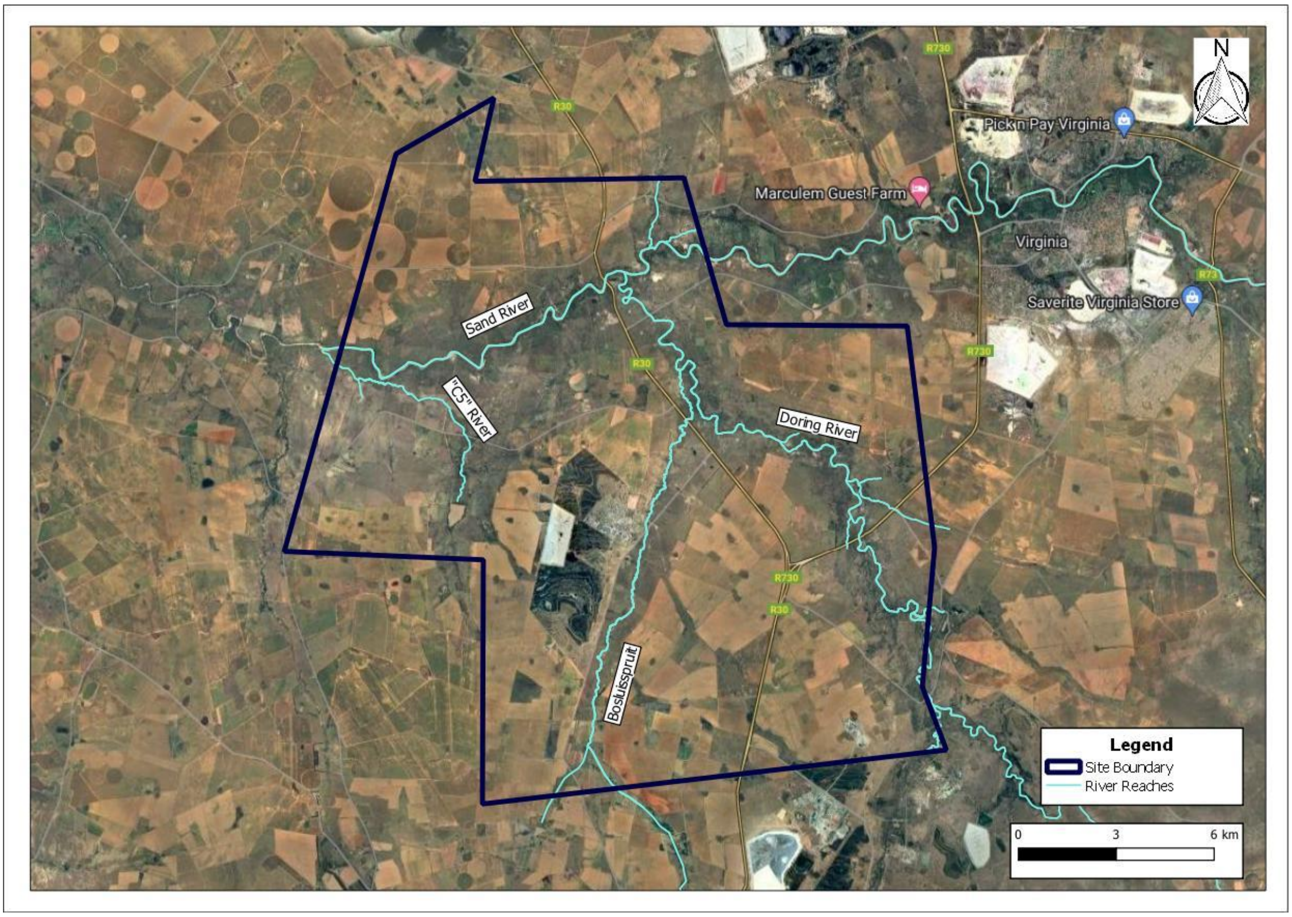

Figure 1-2: Project Area Boundary

The main drainage features traversing the project area include the Bosluisspruit River, Doring River and the Sand River, of which the Sand River is the major system originating in the east and draining south-west past Welkom and through the Project site, refer to Figure 1-2 above.

There are no lakes or dams situated on these rivers mentioned located within the Project Area. The Allemanskraal Dam is located in the middle reaches of the Sand River situated about 45 km upstream of the eastern boundary of the Project Area.

2. Scope of Work

The Scope of Work for the Hydrological Impact Assessment can be summarised as follows:

1. Desktop Assessment:
   - A description of the hydrological baseline receiving environment was prepared based on publicly available data.
   - Identification and description of surface water drainage systems that occur in the study area, and the manner in which these may be affected by the proposed activities were undertaken.
2. Site Visit:
   - A site visit was conducted on 12th and 13th of April 2022 to take measurements of various features and parameters of hydraulic structures and to verify findings of the desktop assessment.
3. Hydrology:
   - The catchment size was assessed, and run-off factors and catchment characteristics were determined.
   - Historical daily rainfall records for the area were sourced.
   - Time of concentration was calculated for each catchment along its longest watercourse, using methods and formulae appropriate to the hydrological method selected.
   - 1:100-year flood peaks were calculated using the most appropriate hydrological methods for each catchment.
4. Hydraulic Modelling:
   - A 1D river hydraulic model was compiled for each of the identified rivers using GeoHEC-RAS river modelling software.
   - Appropriate boundary conditions were selected based on the likely hydraulic regime.
   - The model geometry was based on topographic survey data to be provided by the Client.
   - Roughness factors were determined through an assessment of site and aerial photos.
5. Floodlines:
   - Delineate the floodlines on a map, with respect to any known locations of pipe routes, well locations and plant areas.
6. Risk Assessment:
   - A description of all surface water impacts and proposed mitigation measures, using EIMS' standard EIA Risk and Mitigation methodology.
   - Site sensitivities and relevant potential surface water constraints to the project were identified.
7. Reporting:
   - Recommendations on required hydrological management and mitigation measures will be provided.

The scope of work was expanded on 6th August 2024 following a request for the incorporation of the impact of climate change on the extent of the floodlines developed under this study.

3. Legal Framework

3.1 The EIA study was conducted by EIMS to comply with relevant legislation and policies. The direct applicable guiding legislation is the followingNational Water Act (Act 36 of 1998)

The National Water Act, 1998 (Act No. 36 of 1998) (NWA) is the principal legal instrument relating to water resource management in South Africa. As guardian and trustee of the nation's water resources, the Government (specifically the Department of Water and Sanitation) must ensure that water is protected, used, developed, conserved, managed and controlled in a sustainable and equitable manner for the benefit of all persons and in accordance with its constitutional mandate.

In accordance with GN509 of 2016 as it relates to the National Water Act, 1998 (Act No. 36 of 1998), a regulated area of a watercourse in terms of water uses as listed in Section 21c and 21i is defined as:

- The outer edge of the 1 in 100-year floodline and/or delineated riparian habitat, whichever is the greatest distance, measured from the middle of the watercourse of a river, spring, natural channel, lake or dam;
- in the absence of a determined 1 in 100-year floodline or riparian area the area within 100 m from the edge of a watercourse where the edge of the watercourse is the first identifiable annual bank fill flood bench: or
- A 500m radius from the delineated boundary (extent) of any wetland or pan in terms of this regulation.

3.2 National Environmental Management Act (Act 107 of 1998)

The National Environmental Management Act, 1998 (Act No. 107 of 1998) and the associated Regulations as amended in 2017, states that prior to any development taking place within a wetland or riparian area, an environmental authorisation process needs to be followed. This could follow either the Basic Assessment Report (BAR) process or the Environmental Impact Assessment (EIA) process depending on the scale of the impact. Provincial regulations must also be considered.

3.3 The Constitution of South Africa, 1996

The environment and the health and well-being of people are safeguarded under the Constitution of the Republic of South Africa, 1996 by way of section 24. Section 24(a) guarantees a right to an environment that is not harmful to human health or well-being and to environmental protection for the benefit of present and future generations. Section 24(b) directs the state to take reasonable legislative and other measures to prevent pollution, promote conservation, and secure the ecologically sustainable development and use of natural resources (including water and mineral resources) while promoting justifiable economic and social development. Section 27 guarantees every person the right of access to sufficient water, and the state is obliged to take reasonable legislative and other measures within its available resources to achieve the progressive normalization of this right. Section 27 is defined as a socio-economic right and not an environmental right. However, read with section 24 it requires of the state to ensure that water is conserved and protected and that sufficient access to the resource is provided. Water regulation in South Africa places a great emphasis on protecting the resource and on providing access to water for everyone.

3.4 National Environmental Management: Protected Areas Act (No. 57 of 2003)

This Act governs the establishment and management of protected areas. If the gas extraction project is near a protected area, there could be specific regulations regarding the protection of aquatic ecosystems.

3.5 National Environmental Management: Biodiversity Act (No. 10 of 2004)

This Act could apply if the gas extraction activities are in ecologically sensitive areas, such as wetlands or riparian zones that are hydrologically linked to the surrounding environment.

3.6 Water Services Act, 1997 (Act No. 108 of 1997)

Regulates water supply and sanitation services, particularly where gas operations may affect local water access. Any entity affecting water supply—such as gas companies drilling near water sources—may require authorization from relevant water authorities.

4. Hydrological Characteristics

The project area is located within the Water Management Area 6 of South-Africa, refer to Figure 4-1.

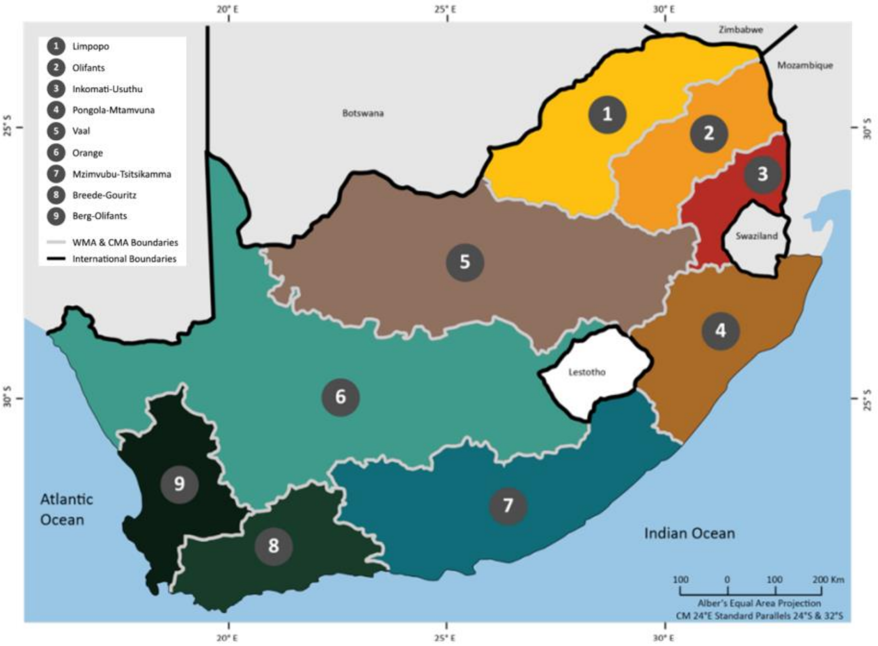

Figure 4-1: The Water Management Areas of South Africa (Source: DWS, April 2016)

The project area is further located within quaternary catchments C42J, C42K, C42L and C43B as defined by Water Resources of South Africa, 2012 study (WR 2012). Refer to Figure 4-2 for the location of the project areas in relation to the quaternary catchments.

Figure 4-2: Project Area in relation to Quaternary Catchments C42J, C42K, C42L and C43B.

The main drainage features traversing the project area include the Bosluisspruit River, Doring River and the Sand River, of which the Sand River is the major system originating in the east and draining south-west past Welkom and through the Project site.

Based on the observations made from Google Earth Pro satellite imagery (Google Earth, 2022) and the site visit that was conducted on the 13th of April 2022, the project area comprises mostly of farmlands with some bush areas in-between. In general, based on the available topographic survey data, the project area is generally flat (<10% slope). A flat topography means the hydrological response of the catchment to rainfall is slower than a catchment with a steeper slope meaning that the flood timing and peak flow characteristics are different to a similar size but steeper catchment.

According to the "SANRAL Drainage Manual, 6th Edition", the soils in the project area have a moderately low to moderately high internal drainage capacity and generalised SCS soil grouping classification for South Africa. Soils that are well drained produce a lower stormflow response than poorly drained soils.

Although the project area and its river section contained within it covers several quaternary catchments, it is really the specific sub-catchments within these quaternary catchments that are important for the flood analysis in question here. The delineation of catchment areas draining to the above-mentioned rivers was undertaken using the topography of the area defined by SRTM DEM data. A catchment area is generally defined as that area from which all rainfall will drain into a drainage system through surface flow, to a common point.

The focus of the reporting within this section is on the major points of the major rivers in the project area. However, the project area has multiple small tributaries that drain into the major rivers at multiple points. To account for this, these were individually considered as flow change locations in the river modelling. This was done so that the peak flow at the downstream end of a river does not represent the entire rivers flow characteristics.. The catchment areas are shown below:

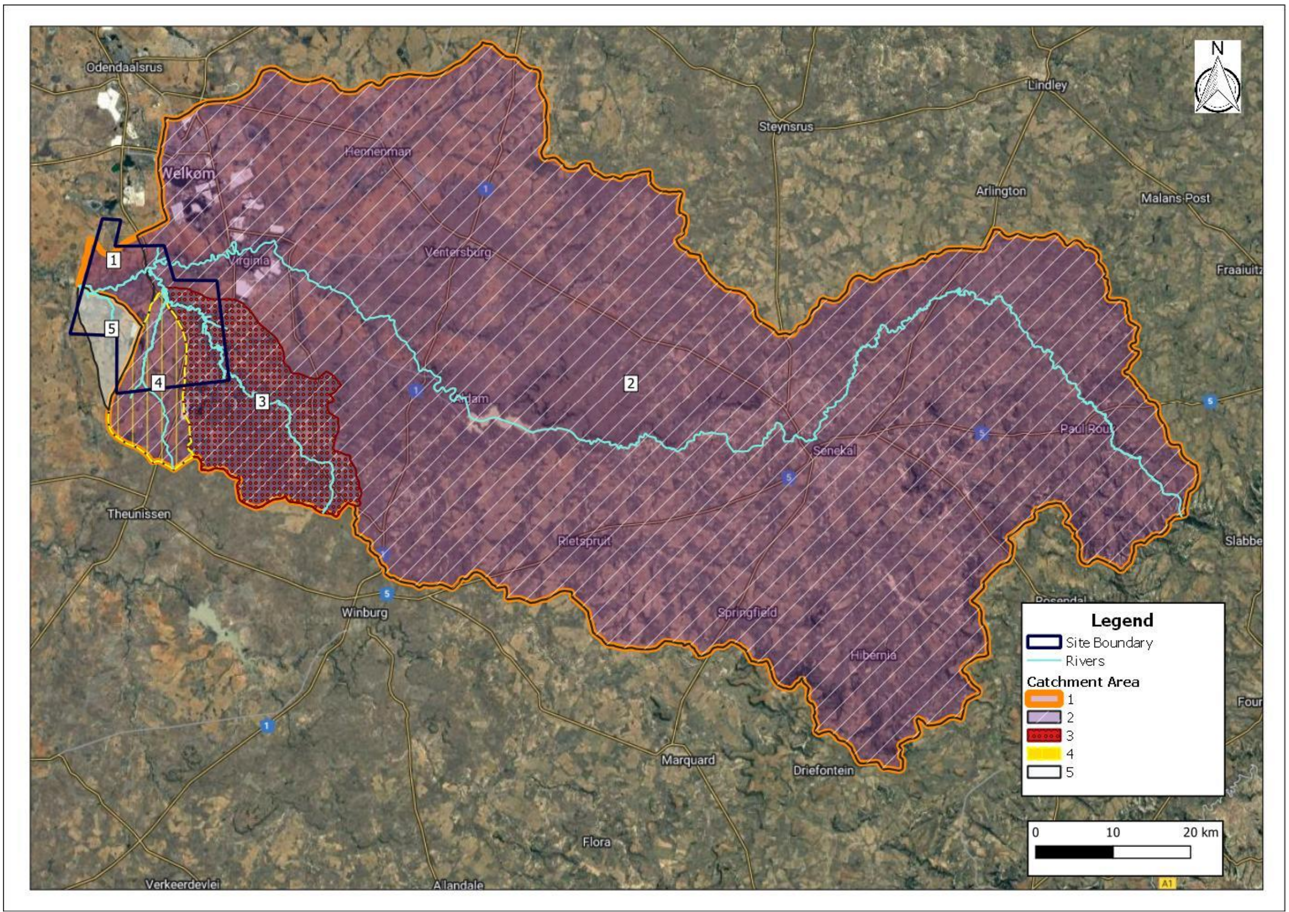

Figure 4-3: Catchment Areas

The physical properties of the various catchment areas shown in Figure 4-3 and are summarized in Table 4-1.

Table 4-1: Catchment Area Physical Properties

Description	Unit	1	2	3	4	5
Size of Catchment Area	km^2	7118	7054	442	155	68
Hydraulic length of Catchment	km	251	217	58	29	20
Average Stream Slope	m/m	0.0013	0.0012	0.0032	0.0055	0.0079

5. Hydrological Analysis

5.1 Methodology

The following methodology was used in the hydrological analysis to determine flood peaks:

- Five flood estimation methods were selected as relevant to the catchment areas under consideration, being the Standard Design Flood Method (SDF), Rational Method (RM), Alternative Rational Method (ARM), Unit Hydrograph Method (UHM) and the Empirical Method developed by Midgley and Pitman.
- Table 3.2 from the SANRAL Drainage Manual shown in Figure 5-1 indicates the applications and limitations of the flood estimation methods.

Method	Input data	Recommended maximum area (km²)	Return period of floods that could be determined (years)	Reference paragraph
Statistical method	Historical flood peak records	No limitation (larger areas)	2 – 200 (depending on the record length)	3.4
Rational methods	Catchment area, watercourse length, average slope, catchment characteristics, design rainfall intensity (3 alternative methods)	Usually < 15, depends on method of calculating rainfall intensity	2 – 200, PMF	3.5.1
Unit Hydrograph method	Design rainfall, catchment area, watercourse length, length to catchment centroid (centre), mean annual rainfall, veld type and synthetic regional unit hydrographs	15 to 5000	2 – 100, PMF	3.5.2
Standard Design Flood method	Catchment area, watercourse length, slope and SDF basin number	No limitation	2 – 200	3.5.3
SCS-SA method	Design rainfall depth, catchment area, Curve Number=f(soils, land cover), catchment lag	< 30	2 - 100	3.5.4
Empirical methods	Catchment area, watercourse length, distance to catchment centroid, mean annual rainfall	No limitation (larger areas)	10 – 100, RMF	3.6

Figure 5-1: Table 3.2 extracted from the SANRAL Drainage Manual

- Input data for these methods was developed as follows:
  - Design rainfall depths were obtained from Water Research Commission Project Number K5/1060 (2002) for Welkom/Sandvet Station (South African Weather Bureau (SAWB) Number 0328308A) for the majority of small catchment areas inside the project area. For the larger catchment areas (1 and 2) that fall within multiple rainfall stations, an average of the MAPs was considered using the arithmetic mean method.
  - The considered rainfall stations are:

    (i) Paul Roux (SAWB No. 0330797W) with MAP of 614mm;

    (ii) Senekal (SAWB No. 0553762 W) with MAP of 625mm;

    (iii) Ventersberg (SAWB No. 0329215W) with MAP of 546mm; and the

    (iv) Welkom/Sandvet (SAWB No. 0328308A) with MAP of 496mm.

    (v) These stations have an average record of 80 years between them.

- The catchment area was delineated using the 30 m SRTM DEM topographical data, using QGIS software.
- The project area is located in SDF Basin number 7, Veld type zone 4 and Kovács region K4.
- The design flood peaks for various return periods were then estimated for both methods using the above inputs. The Utility Programs for Drainage Software (from University of Pretoria) was used to calculate the flood peaks. The program was developed specifically for South African rainfall conditions.

5.2 Topographical Data

The client provided a topographic survey of the project area.

The survey data that was provided for this project was 1 m contours data, providing sufficient accuracy for the scale of the project. The name of the data file used was "Tetra_Virginia_20211102_All Contours" and was received on the 1st of February 2022.

Note: The water depth maps provided in this study are only as accurate as the quality of the topographical data provided, however SMEC took all the necessary steps to apply best engineering judgment to produce the flood maps as accurately as possible.

5.3 Climate Data

5.3.1 Current Climate Conditions

The climate of the study area is characterised by dry winters and wet summers. The warmest months in the region occur between November and February and the coldest months occur between May and August.. Average annual maximum temperature is approximately 28 ^{o}C per annum, according to the National Centre for Environmental Information (NCEI). The main characteristics are shown in Table 5-1 below:

Table 5-1: Long-term average minimum and maximum temperatures

Month	Max. Temp (^{o}C)	Min. Temp (^{o}C)
Jan	32	17
Feb	32	17
Mar	30	15
Apr	27	11
May	24	6
Jun	20	3
Jul	20	2
Aug	24	5
Sep	28	9
Oct	30	13
Nov	31	14
Dec	32	16
Average	**28**	**11**

The Witbank/Sandvet rainfall station is located approximately 8 km north from the centre of the project area. The Mean Annual Precipitation (MAP) for the project area is 496 mm based on the Witbank/Sandvet rainfall station data. This station has a 60-year record. This station was applied to peak flow calculations involving the smaller catchment areas (3, 4 and 5) nearest to the station. Catchment areas 1 and 2 fall within multiple rainfall stations, therefore an average MAP (580 mm) and rainfall depth was applied between all the relevant stations (See Section 5.1). The 24-hour storm rainfall depths for various return periods at the stations are presented in Table 5-2.

Table 5-2: Design Rainfall - 24-hour Rainfall Depths at Rainfall Stations within the Project Area (mm)

Rainfall Station	Return Period (years)					
	2	5	10	20	50	100
Paul Roux	52	69	81	93	100	123
Senekal	48	64	76	87	103	115
Ventersberg	48	64	76	88	104	117
Welkom/Sandvet	51	69	82	94	111	124
Average	**50**	**67**	**79**	**91**	**105**	**120**

5.3.2 Future Climate Conditions

5.3.2.1 Baseline Climate

The following information on climate change was provided by Airshed appointed for Climate Change Expert Services on the project.

Climate change metrics focused on temperature; the number of very hot days (where the maximum temperatures exceed 35°C); rainfall and extreme rainfall events (more than 20 mm of rain occurring within 24 hours).

The baseline (1961 to 1990) annual averages for these metrics were accessed for the area near the project site from the South Africa 'Green Book' (CSIR, 2019). The metrics include three percentiles (10^{th}, 50^{th}, and 90^{th}) as an indication of the variability within the measured data set.

The baseline annual average temperature was in the range 16.1°C (10^{th} percentile) and 16.3°C (90^{th} percentile)) with the number of very hot days varying between 2 (10^{th} percentile) and 4.5 (90^{th} percentile) days per year. The annual average rainfall range between the 10^{th} and 90^{th} percentiles is 1 079 mm and 1 168 mm. Extreme rainfall days varied between 12.4 (10^{th} percentile) and 13.8 (90^{th} percentile) days per year.

Recent change in climatic conditions near the project site were accessed from MeteoBlue a weather forecasting platform developed at the University of Basel, Switzerland. Based on a point selected over the project site, an increasing trend in the annual average temperatures have been observed from 16.9°C in 1979 to 17.5°C in 2023. The change in rainfall over the same period (1979 – 2023) displays a slight decreasing trend from 646 mm in 1979 to 555 mm in 2023.

5.3.2.2 Projected Climate Change

The projected climate change is modelled using Representative Concentration Pathways (RCP).

RCP 4.5 is described by the Intergovernmental Panel on Climate Change (IPCC) as a moderate scenario in which emissions peak around 2040 and then decline. It assumed that effective mitigating measures will be implemented.

RCP 8.5 is the highest baseline emissions scenario in which emissions continue to rise throughout the twenty-first century. It should be noted that current conditions and emissions are tracking closely to the RCP 8.5 pathway, indicating a trajectory towards higher greenhouse gas concentrations and more pronounced climate impacts in the future.

5.3.2.2.1 RCP4.5 Trajectory

The Green Book (CSIR. 2019. Green Book: Adapting South African settlements to climate change. Available at: www.greenbook.co.za) projected temperature changes in the near future (2021 to 2050) indicate a 50th percentile increase of 2.3°C and a 90th percentile increase of 2.8°C (Engelbrecht, et al., 2019). The number of very hot days are expected to increase by 9.7 days per year (50th percentile) to 15.1 days per year (90th percentile). Between 2021 and 2050 the **annual rainfall near the project site is projected to increase by 180 mm** (50th percentile)

(Engelbrecht, et al., 2019), with extreme rainfall days potentially increasing by 1.7 days (50th percentile) in the near future (Engelbrecht, et al., 2019).

5.3.2.2.2 RCP8.5 Trajectory

The Green Book projected temperature changes in the near future (2021 to 2050) indicate a 50th percentile increase of 2.6°C and a 90th percentile increase of 3.2°C (Engelbrecht, *et al.*, 2019). The number of very hot days are expected to increase to 17.1 days per year (50th percentile. Between 2021 and 2050 the **annual rainfall near the project site was projected to increase by 200 mm** between 2021 and 2050 (50th percentile) (Engelbrecht, *et al.*, 2019), with extreme rainfall to increase by 1.5 days (Engelbrecht, *et al.*, 2019).

This trajectory suggests that the expected increase will realize over the intermediate-term period (approximately 30 years). It is not every year that will have the increase, but rather over that period the annual rainfall could go up by 180-200 mm.

Conclusion

Both the RCP 4.5 and RCP 8.5 scenarios project similar increases in MAP over the next 30 years. Given this convergence in projected rainfall trends, a uniform increase of 200 mm has been adopted as a representative estimate. This adjustment is considered to effectively capture the potential climate change impacts on rainfall within the project area, reflecting the influence of both emission pathway trajectories. By using this approach, the analysis ensures a balanced and comprehensive assessment of future hydrological conditions, accounting for projected climate variability under both moderate and high-emission scenarios.

5.4 Adjustment for Climate Change

When assessing the impacts of climate change on floodlines, it is important to understand what the likely impact of climate change is on the peak flow rates generated by rainfall events. Flow rates directly impact the extent of floodlines and must be assessed under climate change conditions then.

For this reason, it is then important to understand the main parameters that impact the value of peak flows/runoffs as determined using rainfall/runoff models.

The most common and widely accepted rainfall/runoff model used in South-Africa and Internationally as well, is the Rational Method, which also forms the basis of the SDF method used and selected for the design case on this project.

The Rational Method is a simple formula stating that the peak flow/runoff (Q-value) is a function of three main parameters, i.e. the catchment characteristics or C-value, the rainfall intensity or I-value and the area of the catchment or A-value. When these are multiplied (using appropriate units), the peak flow rate Q is determined, refer to Equation 5-1: Rational Method Formulae

for the Rational Method Formulae.

$$Q = C\,i\,A$$

Equation 5-1: Rational Method Formulae

For South-Africa, the Rational Method has been calibrated whereby the catchment characteristic (C-value) is a function of the Mean Annual Precipitation (MAP) of the catchment. Since the climate change studies discussed earlier, suggest an increase in the MAP for the Project Area, there is therefore an expected increase in the catchment characteristic C-value for the catchment too. For example, higher MAP areas have typically higher soil moisture content and therefore higher runoff resulting from rainfall. Higher runoff means an increase in stream flow rates and therefore floodlines of larger extent.

Refer to the next chapter for the calculation of the derived impact of Climate Change (higher MAP) on the C-value and therefore the peak flows.

Over and above the relationship between the MAP and the C-value, the Consultant has illustrated that there is also a relationship between the MAP and the rainfall depth and thus rainfall intensity (I-value) in the Rational Formulae. This relationship means a relationship between the runoff/peak flow (Q-value) and climate change through the MAP rainfall depth/intensity relationship.

Refer to the next chapter where it is illustrated how both the C-value and the I-values of the Rational Method was correlated with the mean annual precipitation and therefore a Rational Method based assessment of the impacts of climate change on the runoff/peak flows for the Project Area.

5.4.1 MAP vs 100 Year 24-hour Rainfall Depth

5.4.1.1 Increase in Rainfall Depth

The relationship between the MAP and the 100 year 24-hour rainfall depth as determined in Table 5-3 and Figure 5-2 below was used to adjust the 24-hour rainfall depth for the anticipated higher MAP as projected by Climate Change Studies.

Table 5-3: Weather Station Data - (Design Rainfall Depths at Selected Stations in South Africa – SA Weather Buro)

Weather Station	MAP	Years of Record	100-year 24-hour rainfall depth
Paul Roux	614	73	123
Smaldeel	638	44	119.6
Duikfontein	638	56	101.7
Leuctra	584	67	118
Manitoba	622	37	125.9
Kaallaagte	668	85	118
Senekal	625	94	115.1
Ina	581	28	122.1
Bethel	538	39	107.7
Mignonette	544	45	114
Trekpad	512	79	106.9
Manitoba ""Brandwacht""	486	34	114
Ventersburg	546	91	117.1
Weltevrede	555	54	108.2
Doornpan	580	49	123.3
W Portsland Cement	531	84	111.9
Fraaiuitzicht	583	26	133.2
Kleininbreek	586	39	111.4

The 24-hour rainfall data from Table 5-3 was correlated against the Mean Annual Precipitation (MAP) for the same rainfall stations resulting in the regression relationship as illustrated in Figure 5-2 below.

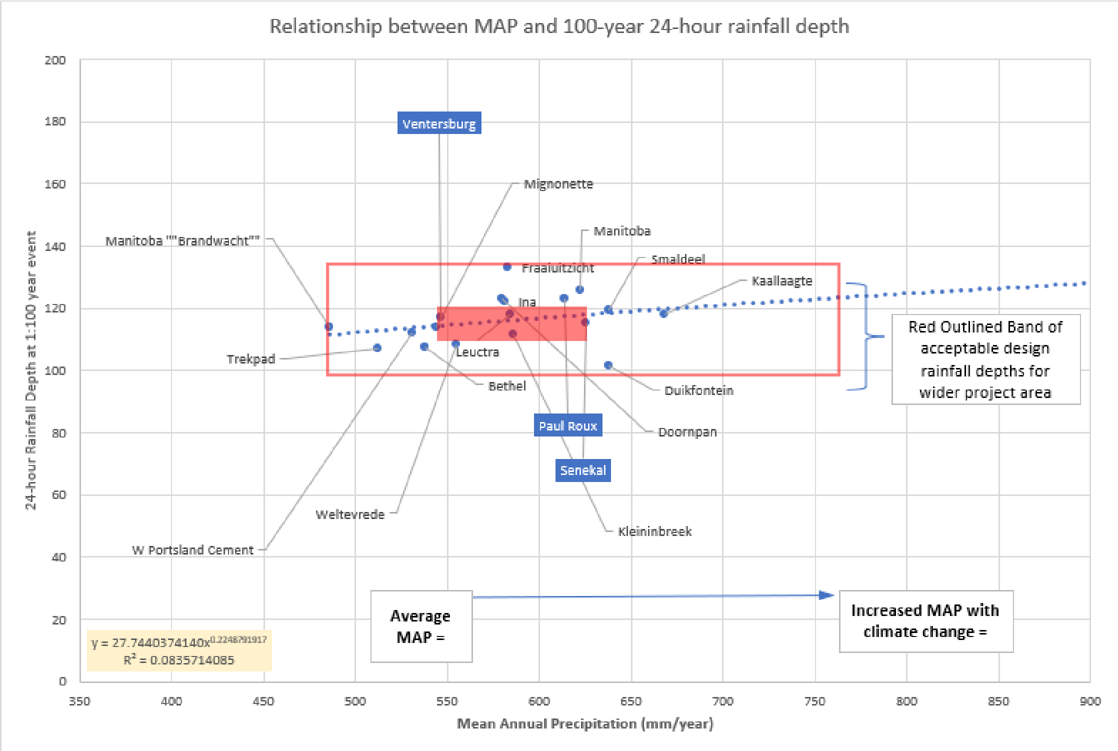

Figure 5-2: Relationship between Rainfall Depth and Mean Annual Precipitation (MAP)

The relationship between the design rainfall and the MAP illustrated that a slight increase in rainfall depth (and therefore rainfall intensity as applied through the Rational Method) can be expected if the Mean Annual Precipitation (MAP) increases as projected by Climate Change Studies.

The relationship between rainfall depth (and thus intensity) and the MAP illustrates that for the anticipated increase in MAP from 550mm/annum to 750mm/annum (increase by 200mm) will result in an increase of 4% in rainfall depth, refer to Table 5-4 for further details.

Table 5-4: Summary of impact of increased MAP on rainfall depth

Description	Magnitude
Average rainfall depth	118.4
Projected Design Rainfall Depth (with climate change)	122.9
Increase in Design Rainfall Depth	**104%**

5.4.1.2 Increase in Run-Off Coefficient

Three factors namely surface slope, ground permeability and vegetation cover and density determine how much of rain is retained on the surface during and after a rainfall event. Separate coefficients are assigned to these three factors as shown in Figure 5-3 below (Table 3C.1 – SANRAL Drainage Manual) making up the combined C-factor as explained earlier with the Rational Method Formulae. The higher coefficients indicate that less of the rainfall is retained and that more rainfall runs off and enters the streams or rivers.

For the Rational Method application, the run-off or catchment characteristic coefficients (C-values) are separated into columns representative of three rainfall ranges. Project areas with a MAP of 600mm and less will be drier, and the ground is expected to absorb more of the initial rainfall than in the higher rainfall area where the ground surface is expected to be already partially saturated at the start of the rain event, resulting in larger runoff and therefore increase runoff/peak flow rates.

Table 3C.1				
Rural (C_1)				
Component	**Classification**	**Mean annual rainfall (mm)**		
		600	**600 - 900**	**900**
Surface slope (C_S)	Wetlands and pans (<3%)	0,01	0,03	0,05
	Flat areas (3 to 10%)	0,06	0,08	0,11
	Hilly (10 to 30%)	0,12	0,16	0,20
	Steep areas (>30%)	0,22	0,26	0,30
Permeability (C_P)	Very permeable	0,03	0,04	0,05
	Permeable	0,06	0,08	0,10
	Semi-permeable	0,12	0,16	0,20
	Impermeable	0,21	0,26	0,30
Vegetation (C_V)	Thick bush and plantation	0,03	0,04	0,05
	Light bush and farm-lands	0,07	0,11	0,15
	Grasslands	0,17	0,21	0,25
	No vegetation	0,26	0,28	0,30

Figure 5-3: Table 3C.1 extracted from SANRAL Drainage Manual

The MAP for the project area before application of climate change falls within the 600mm range but when considering the future up to the year 2050 the MAP increases to a value corresponding with the 600 – 900 mm MAP range. The run-off / catchment characteristic coefficient increases consequently. Total run-off coefficient (C-value or C_1) was adjusted from the 600mm MAP range to the 600-900mm range by applying the Surface Slope (C_S), Permeability (C_P), and Vegetation (C_V) in area proportional ratios to arrive at an overall combined C-factor for the increased MAP under Climate Change Conditions.

The results as shown in Table 5-5 illustrate that an increase in the catchment characteristic (C-value) of up to 40% is expected in future when the Project area is projected to receive a much higher mean annual precipitation.

Table 5-5: Summary of impact of increased MAP on C-value

Description	Magnitude
Calculated C_1 coefficient for current MAP category	0.28
Projected C_1-coefficient for future (2050) MAP category	0.39
Increase in C_1 (Rural) coefficient	**140%**
Net effect from increased rainfall and C_1-coefficient	**146%**

5.4.2 Conclusions on Climate Change Impacts

The climate change metrics provided by Airshed primarily focus on temperature and rainfall. For additional insights, a recent report by S. Schütte, R.E. Schulze, and D.J. Clark, titled "A National Assessment of Potential Climate Change Impacts on the Hydrological Yield of Different Hydro-Climatic Zones of South Africa - Report 1: Methodology and Results," was reviewed. This report affirms the data from Airshed, confirming that higher MAP values are expected in the project area in the future.

Based on this, it is concluded that the projected higher MAP values from climate change studies (RCP 4.5 and RCP 8.5) should guide adjustments to runoff and peak flow values. These adjustments are essential for assessing the impact of climate change on flood levels and flood lines in the future.

Additionally, the well-established relationship between runoff/peak flows and key catchment characteristics—such as the C-value (runoff coefficient) and the rainfall depth/intensity (I-value)—as defined by the internationally recognized Rational Method, which underpins the SDF method, provides a robust framework for evaluating the impacts of increased MAP on flood lines within the project area.

5.4.3 Recommendations on Climate Change Impacts

The recommendation is to therefore to model the river floodlines to reflect a worst-case scenario for annual rainfall increase, i.e. 200mm over the next 30 years, and proceed as below:

i. Increase the annual average rainfall for the 5 catchments by 200mm.

ii. Use the relationship through the Rational Method between the runoff/catchment coefficient (C-value) and the mean annual precipitation to modify the C-value for the corresponding MAP-category in which the Project Area will fall based on future increased MAP.

iii. Use historic relationship between design rainfall (1:100-year event) and MAP to derive a revised design rainfall depth and intensity for the Project Area as a result of climate change.

iv. Adjust the runoff/peak flow in line with adjusted design rainfall and run-off coefficients as explained and determined above. In short, increase the flood estimation values by 146% as determined Table 5-5.

v. Run the GeoHECRAS river models to assess the hydraulic performance of the river sections under the revised flow rates for climate change.

vi. Plot the flood line shifts (due to future increases in MAP) and compare these shifts with the previous flood lines..

5.5 Peak Flow Volumes

5.5.1 Peak Flow Rates Without Climate Change

The peak flows used for floodline determination were calculated using 5 standard methods applied in South Africa shown in Table 5 3. Based on the legislation adopted for this study, peak flows resulting from the 1:100-year event were used in floodline modelling. A summary of the calculated peak flows, for the various catchment areas are presented below and are based on the calculations and inputs indicated in Section 5.1. The peak flow volumes are indicated in Table 5-6 below.

Table 5-6: 1:100-year Peak Flow Rates (m^3/s) – Before Climate Change Impacts

Flood Estimation Method	Peak Flowrates (m^3/s)				
	1	2	3	4	5
Standard Design Flood (SDF)	**3045**	**3022**	**745**	**502**	**325**
Rational Method (RM)	1493	1000	285	188	112
Alternative Rational Method (ARM)	1397	933	242	185	139
Unit Hydrograph Method (UHM)	1267	1258	424	229	134
Midgley and Pitman Empirical Method (EM)	2111	2086	356	213	134

The calculated SDF method flows are generally higher than the other methods. The SDF method was chosen to represent the 1:100-year flood peak at the site. The SDF method resulted in the highest peak flows being estimated for most catchment areas, making its application a conservative / risk averse approach. The SDF method is designed for South African conditions and is one of the most widely used and accepted methods in South Africa (SANRAL, 2013). The method can be accurately applied to catchment areas of any size.. The SDF Method is a development of the internationally accepted Ration Method, calibrated for South Africa.

5.5.2 Peak Flow Rates With Climate Change

The peak flows as reflected in Table 5-6, are therefore increased by 46% or a factor of 1.46 (as calculated in Table 5-5).

The results as shown for the SDF flow rates only, are indicated in Table 5-7.

Table 5-7: SDF - 1:100year Peak Flow Rates (m^3/s) - Projected Climate Change

Flood Estimation Method	Catchments and Peak Flow (m^3/s)				
	1	2	3	4	5
Standard Design Flood (SDF)	**4,456**	**4,402**	**1,088**	**733**	**475**

The increased peak flow rates as calculated above were accordingly introduced into the hydraulic model for assessing the impact on the floodlines, i.e. by how much the floodlines were shifted outwards (wider flow width) as a result of the increased peak flow rates.

The impact of the increased peak flow rates and specifically on the extent of the 1:100 floodlines is illustrated in Section 6.3 (Results) later in this report.

General Comment: Increased flood peaks mean larger land parcels being inundated by flood water, wider flow paths in general and the potential impact to roads, road bridges/culverts as well as infrastructure located along the river in question.

6. Floodline Modelling

The river hydraulics were modelled using the GeoHEC-RAS software suite, developed by CivilGEO Engineering Software. The software utilises the widely used one-dimensional HEC-RAS river hydraulics engine, developed by the US Army Corps of Engineers. The floodlines are based on static flow conditions and do not reflect any additional water rise, due to possible dam break events, in the upstream catchment area. Flood modelling was undertaken for the sections of the above-mentioned rivers that lie within project area boundary.

6.1 Channel Roughness

Channel roughness values are physical parameters describing the irregularity of the surface within a particular stream/river that impacts the water depth, velocity and therefore energy and momentum of water moving from upstream to a downstream location.

Manning’s Roughness coefficient/values (n) were estimated using a visual assessment of Google Earth aerial photograph maps and site photographs. They were based on the description obtained from the SANRAL Drainage manual, 6th Edition as well as the following equation developed by Cowan (1956), to estimate the Manning’s Roughness Coefficient/values (n) for the channel.

$$n = (nb + n1 + n2 + n3 + n4) \times m$$

Where:

nb = a base value of n for a straight, uniform, smooth channel in natural materials
n1 = a correction factor for the effect of surface irregularities
n2 = a value for variations in shape and size of the channel cross section
n3 = a value for obstructions
n4 = a value for vegetation and flow conditions
m = a correction factor for meandering of the channel

Table 6-1: Manning's Roughness Coefficient/values

Parameter	Left Bank	Channel	Right Bank
Sand River	0.111	0.036	0.079
Doring River	0.101	0.040	0.084
Bosluisspruit River	0.099	0.039	0.073
“Catchment 5” River	0.078	0.037	0.078

The values above represent the average Manning’s roughness values across the rivers inside the project area. Generally, every section along a natural river has a different manning’s roughness due to its irregular nature. The following figures indicate the channel characteristics at each of the rivers.

Figure 6-1: Sand River Channel Characteristic

Figure 6-2: Doring River Channel Characteristics

Figure 6-3: Bosluisspriut Channel Characteristics

Figure 6-4: "Catchment 5"River Channel Characteristics

6.2 River Hydraulic Model

A site visit of the culverts and bridges was conducted on the 12th and 13th of April 2022 by SMEC. During this site visit, the dimensions for bridges and culvert structures, considered/included in the hydraulic river model, were measured.

A total of three bridges and eight road culverts were surveyed/measured and were incorporated in the hydraulic model to ensure an accurate representation of the floodlines in these vicinities were provided. Weir structures/ dams that were present within the river sections were deemed minor from a hydraulic constriction perspective and were not included in the hydraulic analysis since these have minor impacts on the flood levels in general.

Figure 6-5 indicates the locations of the hydraulic structures that were measured.

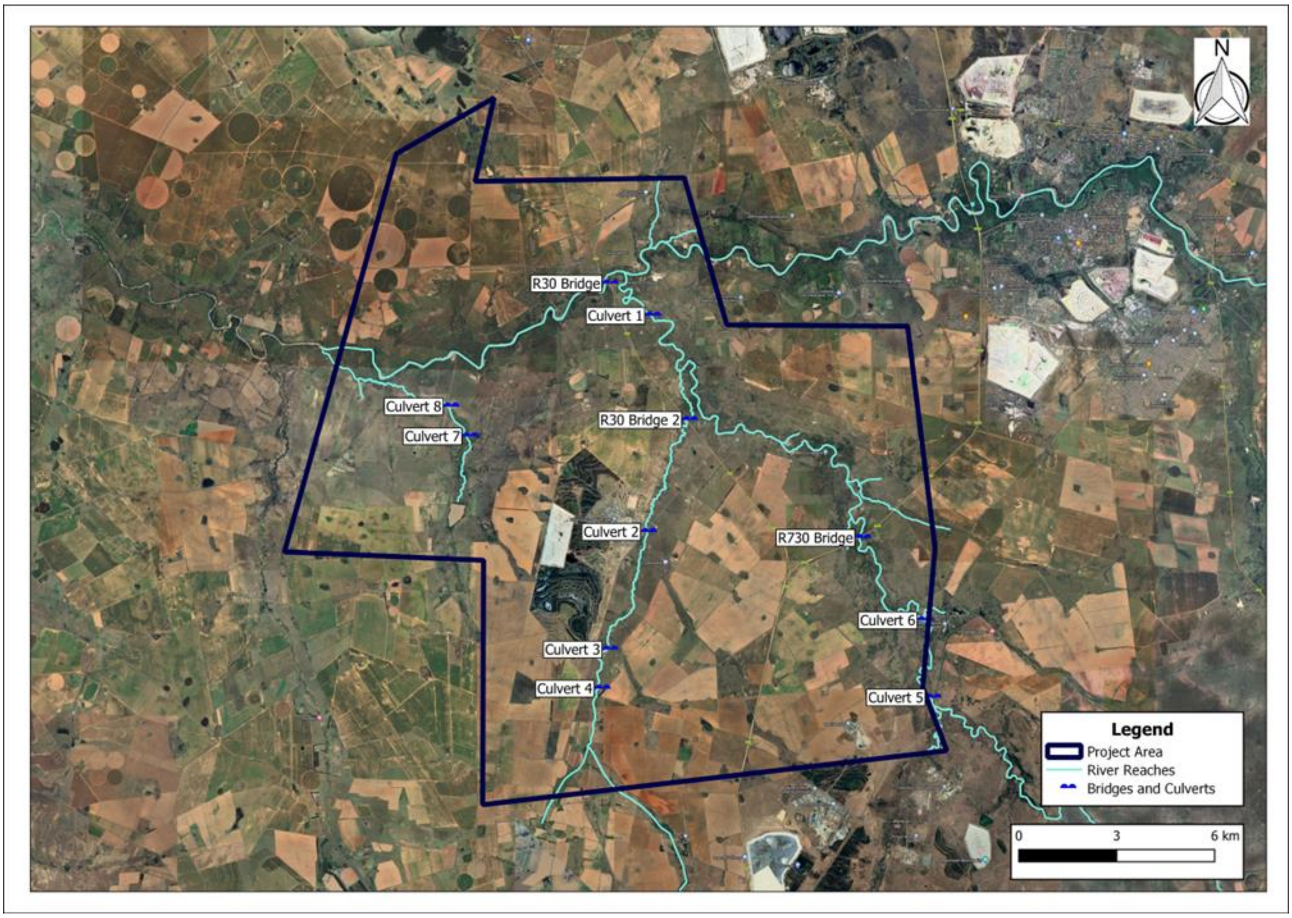

Figure 6-5: Bridges and Culverts Locations

6.2.1 Boundary Conditions

The normal depth condition was used as the downstream and upstream hydraulic controls / boundaries. In general, the boundary condition assumption had little to no effect on the flood depth, near the project area. It did however make a difference on the downstream boundary of the Sand River. Increasing or reducing the slope affects the position of floodlines. The average slope of the river was assumed as the downstream boundary. The downstream boundary slope used was the average slope of the river inside the project area.

6.3 Results

The peak flows estimated by the SDF method as presented in Section 5 were used to simulate the floodlines of the rivers running through the Tetra4 Gas project area. The floodlines are indicated in Figure 6-6, below. Refer to Appendix C for a larger image.

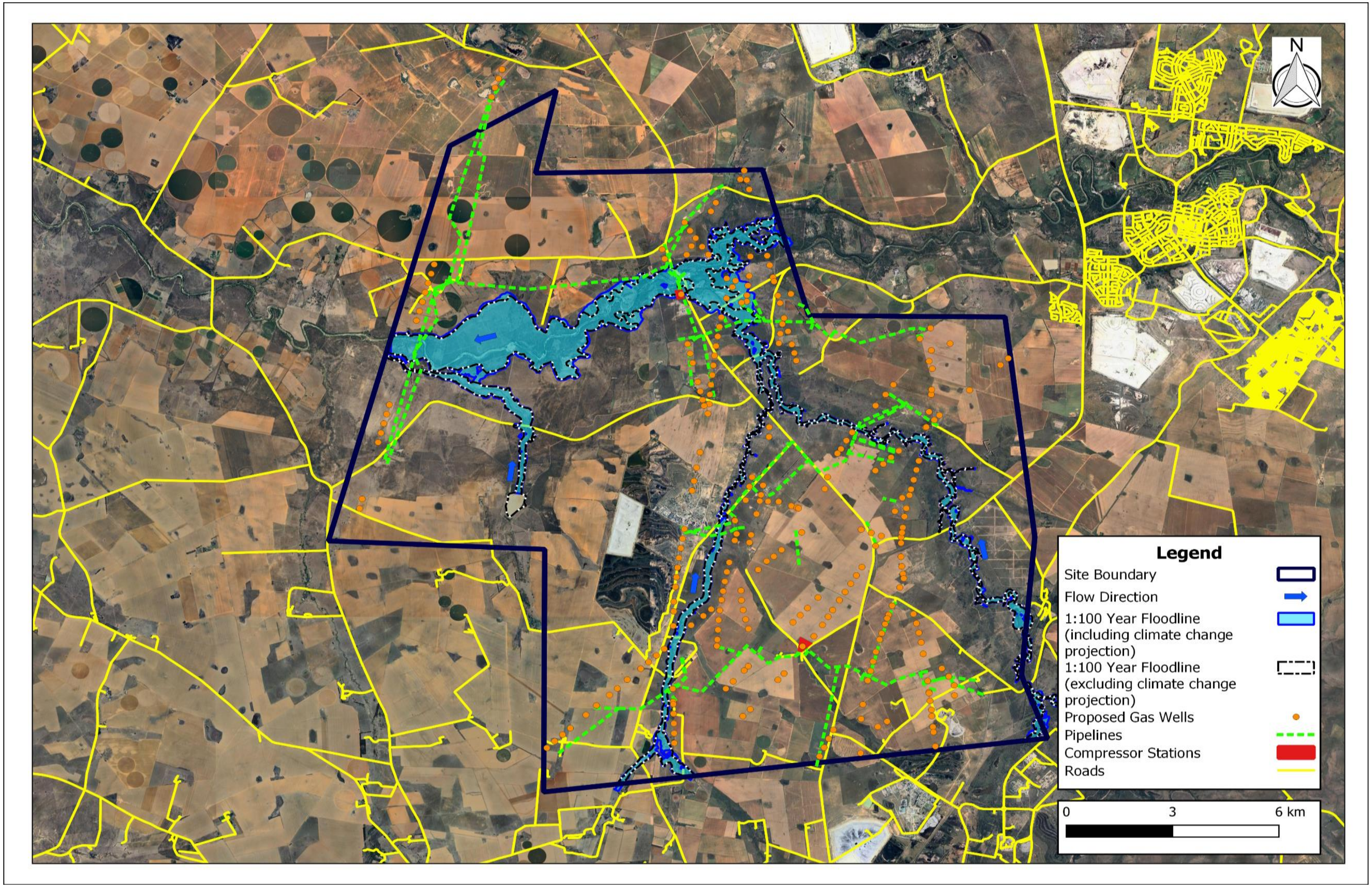

Figure 6-6: 100-Year Floodlines With and Without Climate Change.

7. Site Sensitivities

The sensitivities and constraints at the Tetra4 Cluster 2 Gas project site were assessed in accordance with the National Water Act Regulations (GN509, 2016) and the EIMS sensitivity assessment methodologies. Based on the National Water Act (GN509, 2016) described in Section 3, the area within the 1:100-year floodline is considered to be highly sensitive. A well site may not be located within the 1:100-year floodline. Map indicates a sensitivity map which was developed to assist in identifying sensitive features in relation to the 1:100-year flood within the project area with consideration for climate change impacts.

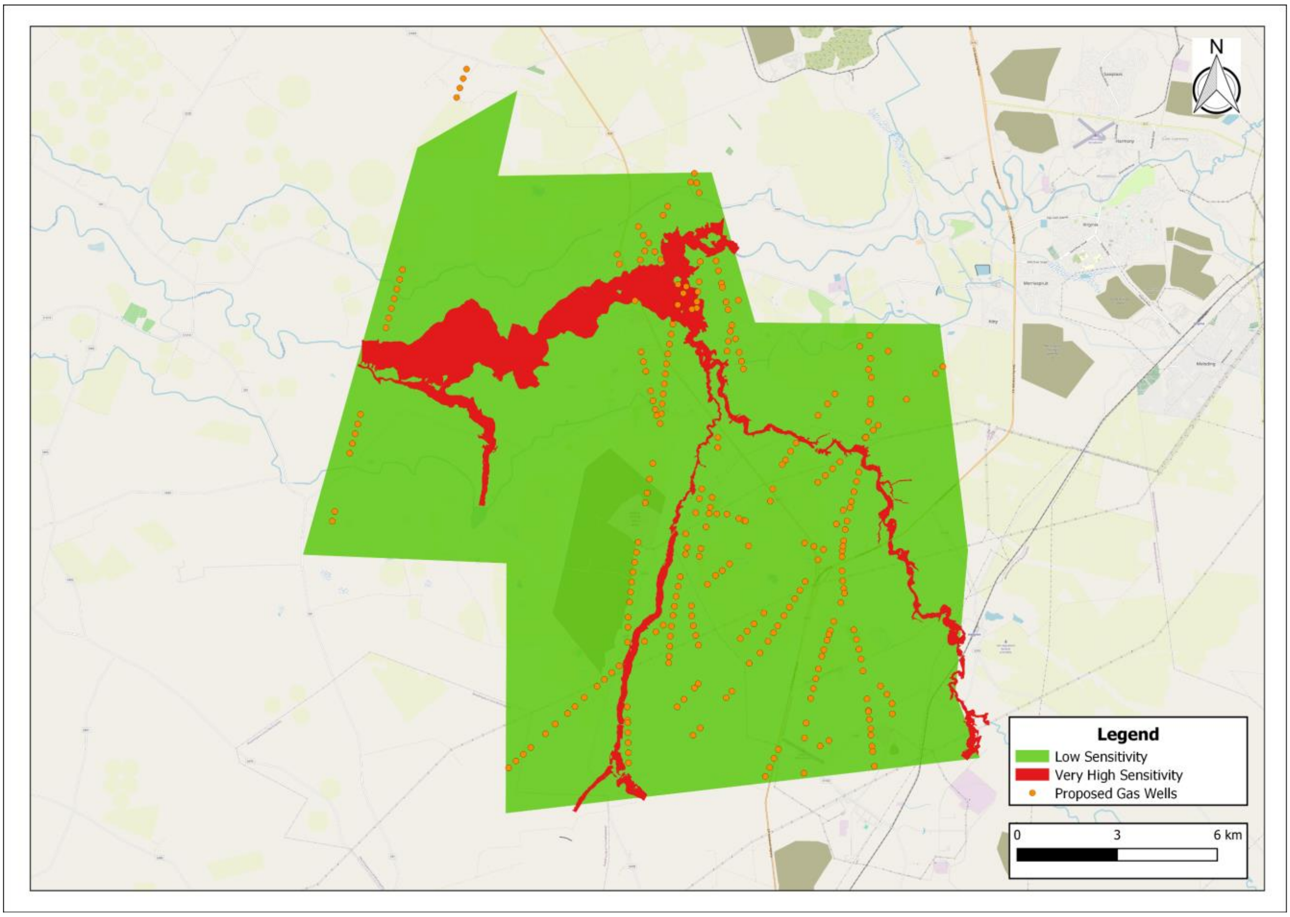

Figure 7-1: Hydrology Sensitivity Map

According to Figure 7-1 there is an estimated 8 gas wells located within the very high sensitivity area (1:100-year floodline) of the project which would form part of the overall analysis and approval of placing final well infrastructure to be determined by the Client/Developer.

8. Potential Impacts and Mitigation

This section presents the flowing:

- Potential impacts on the ecology of the identified watercourses associated with the proposed development.
- Recommended mitigation measures needed to minimise the perceived impacts of the proposed development.

Most impacts are considered to be easily detectable and the considered mitigation measures are easily practicable therefore the risks associated with the development are considered to be low.

8.1 Construction Phase Impacts

During the construction phase, pipes connecting the new wells to the compressor stations and helium plant will be laid down. Construction work for laying of pipes across rivers or parallel to them may involve the excavation of riverbed material and restoring the river to a near-natural state thereafter. Horizontal Directional Drilling (HDD) will be the method generally used on site to lay pipes so that the impact is minimal/negligible.

Table 8-1: Construction Phase Impacts and Mitigation Measures

Potential Impacts	Mitigation Measures
Exposure of soil, leading to increased runoff, and erosion, and thus increased sedimentation of the watercourses.	Ensure total footprint area is kept to a minimum.
	Traffic and movement of machinery should be minimised and restricted to certain paths.
	Progressive rehabilitation of disturbed land should be carried out.
Soil and stormwater contamination by oils and hydrocarbons spills, originating from construction vehicles	Construction waste must be collected and stored safely for disposal in accordance with the relevant waste regulations, protocols, and product specifications. Care must be taken not to leave any waste in the project area that can lead to future contamination of the project area or the downstream area.
Increase in the number of alien and/or invasive vegetation because of disturbances.	Monitoring of the project area for alien and invasive vegetation species must be undertaken, specifically near access roads through or along the watercourses. Should alien and invasive plant species be identified, they must be removed and disposed of as per an alien and invasive species control plan and the area must be revegetated with suitable indigenous vegetation.
Alterations of the riverbanks and riverbed due to movement near the drainage lines.	The reaches of all watercourses where no construction activities are planned to occur must be considered no-go areas.
Wastewater discharge to nearby water source, posing risks to ecosystems and human health.	During construction a stormwater management plan to be drawn up and approved for managing surface runoff from disturbed land/construction activities, these may include attenuation dams and silt traps.
	Wastewater (sewage) to be managed on site through either on-site treatment to acceptable effluent standards for release to environment or alternatively

Potential Impacts	Mitigation Measures
	trucked off-site and disposed of at approved wastewater treatment works in the area.

8.2 Operational Phase Impacts

The activities expected during the operational phase involve the operation of the well pad, pipelines, compression station and LNG/LHe beneficiation plant, movement of trucks and other vehicles, general and hazardous waste management, gas processing as well as operation of road tankers for gas distribution. The potential environmental impacts and mitigation measures during the operational phase are listed below.

Table 8-2: Operational Phase Impacts and Mitigation Measures

Potential Impacts	Mitigation Measures
Disturbance to soil and ongoing erosion as a result of periodic maintenance activities.	No movement of construction equipment through the watercourses may be permitted during standard operational activities or maintenance activities. Use must be made of the existing and/or approved watercourse crossings only.
	Regular conditional inspections of all stormwater infrastructure are required. Inspection data must be recorded and accumulated for tracking purposes. Regular reporting should be scheduled management task.
	Specific attention must be given to inspection during and after any rain and/or flood event to kerb any damage that may have occurred.
Altered water quality as a result of increased availability of pollutants.	Oil recovered from construction vehicles and machinery should be collected, stored, and disposed of by accredited vendors for recycling.
Potential increase in the number of alien and/or invasive vegetation as a result of floods or people who visit the site.	Monitoring for the project area for alien and invasive vegetation species must be undertaken, specifically near access roads through or along the watercourses. Should alien and invasive plan species be identified, they must be removed and disposed of as per an alien and invasive species control plan and the area must be revegetated with suitable indigenous vegetation.

8.3 Decommissioning Phase Impacts

The decommissioning phase involves the removal of all berms, trenches and other storm water infrastructure, stationary infrastructure, pipeline infrastructure and wastes.

Table 8-3: Decommissioning Phase Impacts

Potential Impacts	Mitigation Measures
Increased erosion due to construction vehicles movement.	Topsoil removed during construction must be stored on site for rehabilitation and re-vegetation. The soil must be stabilised using materials such as netting or geotextiles where necessary.

Potential Impacts	Mitigation Measures
	The site shall be re-instated to its original condition as far as possible. No foreign material generated / deposited during construction shall remain on site.
	Rehabilitate disturbance areas as soon as construction in an area is completed.
Stormwater Contamination resulting from spillages of polluted groundwater from wells	All wells should be capped to prevent the spilling of contaminated groundwater.
Potential increase in the number of alien and/or invasive vegetation as a result of floods or people who visit the site.	Monitoring for the project area for alien and invasive vegetation species must be undertaken, specifically near access roads through or along the watercourses. Should alien and invasive plan species be identified, they must be removed and disposed of as per an alien and invasive species control plan and the area must be revegetated with suitable indigenous vegetation.

SMEC South Africa (Pty) Ltd

230 Albertus Street,
Montagne, Pretoria, South Africa, 0184

PO Box 72927 Lynnwood Ridge 0040 South Africa

Phone: +27 12 481 3800

Email: pretoria@smec.com

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Appendix A: Hydrological Calculations

Utility Programs for Drainage
Flood calculations

Project name: Tetra4 Gas Floodline
Analysed by: Rendani Thovhakale
Name of river: Reach 1
Description of site: Catchment 1
Filename: C:\Users\rt2704930\OneDrive - Surbana Jurong Private Limited\Desktop\Desktop\Manager\Tetra4 Gas\Hydrology\Downstream 1 (Catchment 1) .fld
Date: 10 February 2022


```
Flood frequency analysis : Standard Design Flood method

Project name                                 = Tetra4 Gas Floodline
Analysed by                                  = Rendani Thovhakale
Name of river                                = Reach 1
Description of site                          = Catchment 1
Date                                         = 2022/02/10
Catchment characteristics:
Area of catchment                            = 7118 km²
Length of longest watercourse                = 251 km
1085 height difference                       = 251 m
Average slope                                = 0.0013 m/m
Drainage basin characteristics:
Drainage basin number                        = 7
Mean annual daily max rain                   = 49 mm
Days on which thunder was heard              = 39 days
Runoff coefficient C2                        = 15 %
Runoff coefficient C100                      = 60 %
Basin mean annual precipitation              = 510 mm
Basin mean annual evaporation                = 1700 mm
Basin evaporation index MAE/MAP              = 3.33
```

RAINFALL DATA
The rainfall data in the table below are derived from two sources. The daily rainfall is from the Department of Water Affair's publication TR102 for the representative site. The modified Hershfield equation is used for durations up to four hours. Linear interpolation is used for values between 4 hours and one day.

Weather Services station ex TR102 = 328726 @ OLIVINE
Point mean annual precipitation = 510 mm

Dur:	RP =2	5	10	20	50	100	200
.25 h	14	24	32	39	49	57	64
.50 h	19	32	41	51	64	74	84
1 h	23	39	51	63	79	91	103
2 h	27	46	61	75	94	108	122
4 h	32	54	70	87	109	125	142
1 day	49	68	82	96	118	137	157
2 days	62	87	107	128	158	184	213
3 days	68	94	115	136	167	193	221
7 days	84	118	144	172	211	243	279

Runoff coefficients C2 = 15 % C100 = 60 %

Return period (years)	Time of concentration (hours)	Point precipitation (mm)	ARF (%)	Catchment precipitation (mm)	Runoff coefficient (%)	Peak flow (m³/s)
1:2	59.75	48.8	79.8	39.0	15.0	193.56
1:5	59.75	82.4	79.8	65.7	31.2	679.70
1:10	59.75	107.7	79.8	86.0	39.7	1131.06
1:20	59.75	133.1	79.8	106.2	46.7	1642.05
1:50	59.75	166.6	79.8	133.0	54.6	2404.59
1:100	59.75	192.0	79.8	153.3	60.0	3045.14
1:200	59.75	217.4	79.8	173.5	64.8	3724.94

Calculated using Utility Programs for Drainage 1.1.0

Utility Programs for Drainage
Flood calculations

Project name: Tetra4 Gas Floodlines
Analysed by: Rendani Thovhakale
Name of river:
Description of site: Catchment 2
Filename: C:\Users\rt2704930\OneDrive - Surbana Jurong Private Limited\Desktop\Desktop\Manager\Tetra4 Gas\Hydrology\R30 Bridge (Catchment 2).fld
Date: 10 February 2022

Flood frequency analysis : Standard Design Flood method

Project name = Tetra4 Gas Floodlines
Analysed by = Rendani Thovhakale
Name of river =
Description of site = Catchment 2
Date = 2022/02/10
Catchment characteristics:
Area of catchment = 7054 km²
Length of longest watercourse = 239 km
1085 height difference = 217 m
Average slope = 0.0012 m/m
Drainage basin characteristics:
Drainage basin number = 7
Mean annual daily max rain = 49 mm
Days on which thunder was heard = 39 days
Runoff coefficient C2 = 15 %
Runoff coefficient C100 = 60 %
Basin mean annual precipitation = 510 mm
Basin mean annual evaporation = 1700 mm
Basin evaporation index MAE/MAP = 3.33

RAINFALL DATA
The rainfall data in the table below are derived from two sources. The daily rainfall is from the Department of Water Affair's publication TR102 for the representative site. The modified Hershfield equation is used for durations up to four hours. Linear interpolation is used for values between 4 hours and one day.

Weather Services station ex TR102 = 328726 @ OLIVINE
Point mean annual precipitation = 510 mm

Dur:	RP =2	5	10	20	50	100	200
.25 h	14	24	32	39	49	57	64
.50 h	19	32	41	51	64	74	84
1 h	23	39	51	63	79	91	103
2 h	27	46	61	75	94	108	122
4 h	32	54	70	87	109	125	142
1 day	49	68	82	96	118	137	157
2 days	62	87	107	128	158	184	213
3 days	68	94	115	136	167	193	221
7 days	84	118	144	172	211	243	279

Runoff coefficients C2 = 15 % C100 = 60 %

Return period (years)	Time of concentration (hours)	Point precipitation (mm)	ARF (%)	Catchment precipitation (mm)	Runoff coefficient (%)	Peak flow (m³/s)
1:2	59.72	48.8	79.9	39.0	15.0	192.06
1:5	59.72	82.4	79.9	65.8	31.2	674.43
1:10	59.72	107.7	79.9	86.0	39.7	1122.29
1:20	59.72	133.1	79.9	106.3	46.7	1629.31
1:50	59.72	166.6	79.9	133.1	54.6	2385.94
1:100	59.72	192.0	79.9	153.4	60.0	3021.53
1:200	59.72	217.4	79.9	173.6	64.8	3696.06

Calculated using Utility Programs for Drainage 1.1.0

Utility Programs for Drainage
Flood calculations

Project name: Tetra4 Gas Floodlines
Analysed by: Rendani Thovhakale
Name of river:
Description of site: Catchment 3
Filename: C:\Users\rt2704930\OneDrive - Surbana Jurong Private Limited\Desktop\Desktop\Manager\Tetra4 Gas\Hydrology\Junction 1 (Catchment 3).fld
Date: 10 February 2022

Flood frequency analysis : Standard Design Flood method

Project name	= Tetra4 Gas Floodlines
Analysed by	= Rendani Thovhakale
Name of river	=
Description of site	= Catchment 3
Date	= 2022/02/10
Catchment characteristics:	
Area of catchment	= 442 km²
Length of longest watercourse	= 58 km
1085 height difference	= 134 m
Average slope	= 0.0031 m/m
Drainage basin characteristics:	
Drainage basin number	= 7
Mean annual daily max rain	= 49 mm
Days on which thunder was heard	= 39 days
Runoff coefficient C2	= 15 %
Runoff coefficient C100	= 60 %
Basin mean annual precipitation	= 510 mm
Basin mean annual evaporation	= 1700 mm
Basin evaporation index MAE/MAP	= 3.33

RAINFALL DATA
The rainfall data in the table below are derived from two sources. The daily rainfall is from the Department of Water Affair's publication TR102 for the representative site. The modified Hershfield equation is used for durations up to four hours. Linear interpolation is used for values between 4 hours and one day.

Weather Services station ex TR102 = 328726 @ OLIVINE
Point mean annual precipitation = 510 mm

Dur:	RP =2	5	10	20	50	100	200
.25 h	14	24	32	39	49	57	64
.50 h	19	32	41	51	64	74	84
1 h	23	39	51	63	79	91	103
2 h	27	46	61	75	94	108	122
4 h	32	54	70	87	109	125	142
1 day	49	68	82	96	118	137	157
2 days	62	87	107	128	158	184	213
3 days	68	94	115	136	167	193	221
7 days	84	118	144	172	211	243	279

Runoff coefficients C2 = 15 % C100 = 60 %

Return period (years)	Time of concentration (hours)	Point precipitation (mm)	ARF (%)	Catchment precipitation (mm)	Runoff coefficient (%)	Peak flow (m³/s)
1:2	14.01	39.7	90.6	36.0	15.0	47.36
1:5	14.01	67.0	90.6	60.7	31.2	166.31
1:10	14.01	87.6	90.6	79.4	39.7	276.75
1:20	14.01	108.3	90.6	98.1	46.7	401.78
1:50	14.01	135.6	90.6	122.9	54.6	588.36
1:100	14.01	156.2	90.6	141.6	60.0	745.09
1:200	14.01	176.8	90.6	160.3	64.8	911.43

Calculated using Utility Programs for Drainage 1.1.0

Utility Programs for Drainage
Flood calculations

Project name: Tetra4 Gas Floodline
Analysed by: Rendani Thovhakale
Name of river:
Description of site: Catchment 4
Filename: C:\Users\rt2704930\OneDrive - Surbana Jurong Private Limited\Desktop\Desktop\Manager\Tetra4 Gas\Hydrology\Junction 2 (Catchment 4).fld
Date: 10 February 2022

Flood frequency analysis : Standard Design Flood method

Project name = Tetra4 Gas Floodline
Analysed by = Rendani Thovhakale
Name of river =
Description of site = Catchment 4
Date = 2022/02/10
Catchment characteristics:
Area of catchment = 155 km^2
Length of longest watercourse = 29 km
1085 height difference = 117 m
Average slope = 0.0054 m/m
Drainage basin characteristics:
Drainage basin number = 7
Mean annual daily max rain = 49 mm
Days on which thunder was heard = 39 days
Runoff coefficient C2 = 15 %
Runoff coefficient C100 = 60 %
Basin mean annual precipitation = 510 mm
Basin mean annual evaporation = 1700 mm
Basin evaporation index MAE/MAP = 3.33

RAINFALL DATA
The rainfall data in the table below are derived from two sources. The daily rainfall is from the Department of Water Affair's publication TR102 for the representative site. The modified Hershfield equation is used for durations up to four hours. Linear interpolation is used for values between 4 hours and one day.

Weather Services station ex TR102 = 328726 @ OLIVINE
Point mean annual precipitation = 510 mm

Dur:	RP =2	5	10	20	50	100	200
.25 h	14	24	32	39	49	57	64
.50 h	19	32	41	51	64	74	84
1 h	23	39	51	63	79	91	103
2 h	27	46	61	75	94	108	122
4 h	32	54	70	87	109	125	142
1 day	49	68	82	96	118	137	157
2 days	62	87	107	128	158	184	213
3 days	68	94	115	136	167	193	221
7 days	84	118	144	172	211	243	279

Runoff coefficients C2 = 15 % C100 = 60 %

Return period (years)	Time of concentration (hours)	Point precipitation (mm)	ARF (%)	Catchment precipitation (mm)	Runoff coefficient (%)	Peak flow (m^3/s)
1:2	6.63	35.0	93.4	32.7	15.0	31.89
1:5	6.63	59.1	93.4	55.2	31.2	111.97
1:10	6.63	77.3	93.4	72.2	39.7	186.33
1:20	6.63	95.5	93.4	89.2	46.7	270.51
1:50	6.63	119.5	93.4	111.6	54.6	396.13
1:100	6.63	137.7	93.4	128.6	60.0	501.66
1:200	6.63	155.9	93.4	145.6	64.8	613.65

Calculated using Utility Programs for Drainage 1.1.0

Utility Programs for Drainage
Flood calculations

Sinotech

Project name: Tetra4 Gas Floodline
Analysed by:
Name of river:
Description of site: Catchment 5
Filename: C:\Users\rt2704930\OneDrive - Surbana Jurong Private Limited\Desktop\Desktop\Manager\Tetra4 Gas\Hydrology\Downstream 2 (Catchment 5).fld
Date: 10 February 2022

Flood frequency analysis : Standard Design Flood method

Project name = Tetra4 Gas Floodline
Analysed by =
Name of river =
Description of site = Catchment 5
Date = 2022/02/10
Catchment characteristics:
Area of catchment = 68.2 km²
Length of longest watercourse = 20.5 km
1085 height difference = 117 m
Average slope = 0.0076 m/m
Drainage basin characteristics:
Drainage basin number = 7
Mean annual daily max rain = 49 mm
Days on which thunder was heard = 39 days
Runoff coefficient C2 = 15 %
Runoff coefficient C100 = 60 %
Basin mean annual precipitation = 510 mm
Basin mean annual evaporation = 1700 mm
Basin evaporation index MAE/MAP = 3.33

RAINFALL DATA
The rainfall data in the table below are derived from two sources. The daily rainfall is from the Department of Water Affair's publication TR102 for the representative site. The modified Hershfield equation is used for durations up to four hours. Linear interpolation is used for values between 4 hours and one day.

Weather Services station ex TR102 = 328726 @ OLIVINE
Point mean annual precipitation = 510 mm

Dur:	RP =2	5	10	20	50	100	200
.25 h	14	24	32	39	49	57	64
.50 h	19	32	41	51	64	74	84
1 h	23	39	51	63	79	91	103
2 h	27	46	61	75	94	108	122
4 h	32	54	70	87	109	125	142
1 day	49	68	82	96	118	137	157
2 days	62	87	107	128	158	184	213
3 days	68	94	115	136	167	193	221
7 days	84	118	144	172	211	243	279

Runoff coefficients C2 = 15 % C100 = 60 %

Return period (years)	Time of concentration (hours)	Point precipitation (mm)	ARF (%)	Catchment precipitation (mm)	Runoff coefficient (%)	Peak flow (m³/s)
1:2	4.44	32.5	96.2	31.3	15.0	20.03
1:5	4.44	54.8	96.2	52.8	31.2	70.35
1:10	4.44	71.7	96.2	69.0	39.7	117.06
1:20	4.44	88.6	96.2	85.3	46.7	169.94
1:50	4.44	110.9	96.2	106.8	54.6	248.86
1:100	4.44	127.8	96.2	123.0	60.0	315.16
1:200	4.44	144.7	96.2	139.3	64.8	385.51

Calculated using Utility Programs for Drainage 1.1.0

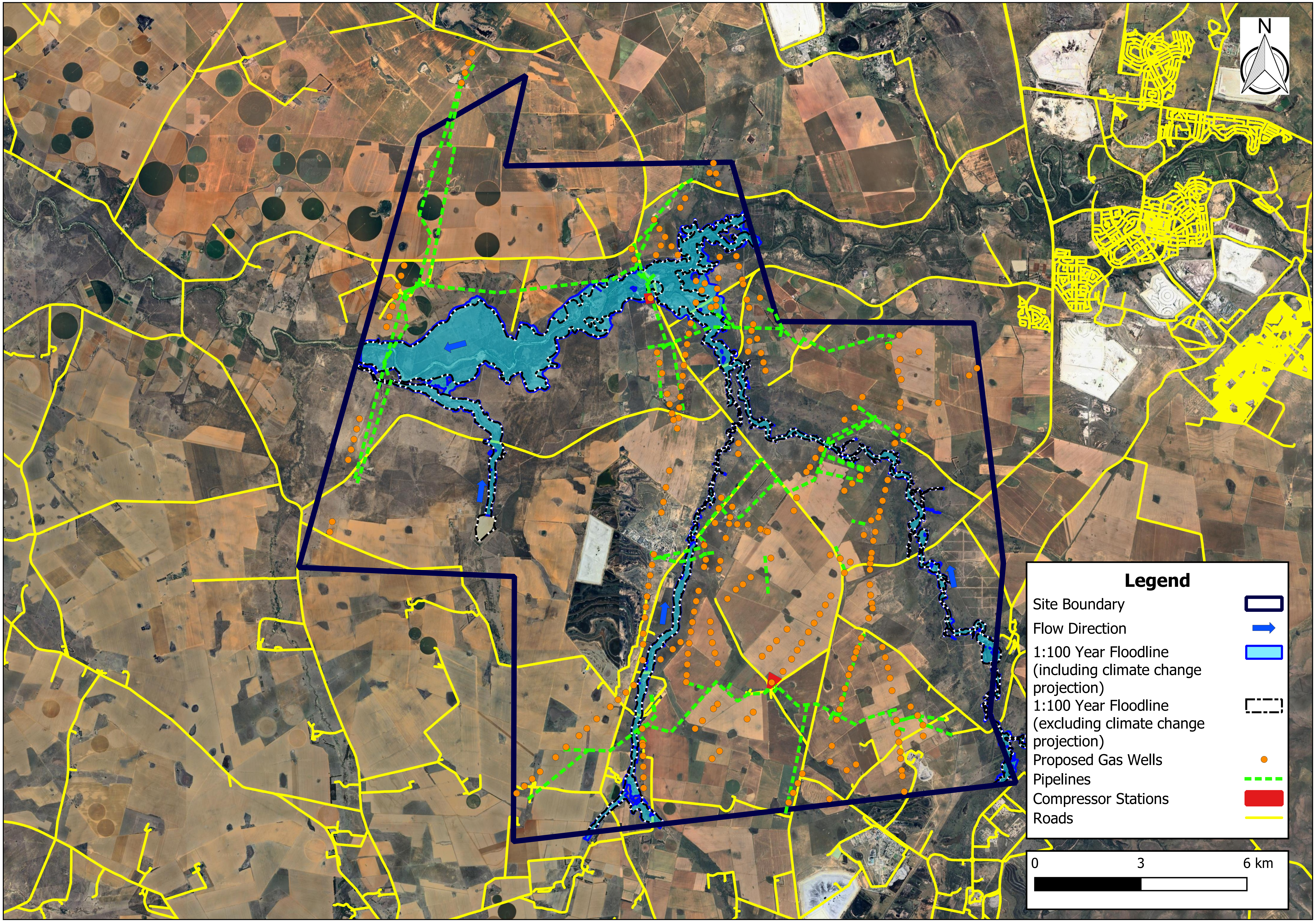
Appendix B: Impact Significance Ratings

IMPACT DESCRIPTION			Pre-Mitigation						
Identifier	Impact	Phase	Nature	Extent	Duration	Magnitude	Reversibility	Probability	Pre-mitigation ER
10.1.1	Loss of watercourse vegetation	Construction	-1	2	1	1	2	2	-3
10.1.2	Erosion	Construction	-1	1	2	1	2	4	-6
10.1.3	Stormwater contamination	Construction	-1	1	2	2	2	4	-7
10.1.4	Alien and/or Invasive Vegetation	Construction	-1	3	4	3	3	2	-6.5
10.1.5	Alterations of the river banks and river bed	Construction	-1	2	2	2	3	3	-6.75
10.1.6	Erosion	Operation	-1	2	4	3	2	2	-5.5
10.1.7	Stormwater contamination	Operation	-1	3	3	3	3	3	-9
10.1.8	Alien and/or Invasive Vegetation	Operation	-1	3	4	3	3	3	-9.75
10.1.9	Erosion	Decommissioning	-1	2	3	3	2	2	-5
10.1.10	Stromwater contamination	Decommissioning	-1	3	3	3	3	3	-9
10.1.11	Alien and/or Invasive Vegetation	Decommissioning	-1	3	4	3	3	2	-6.5

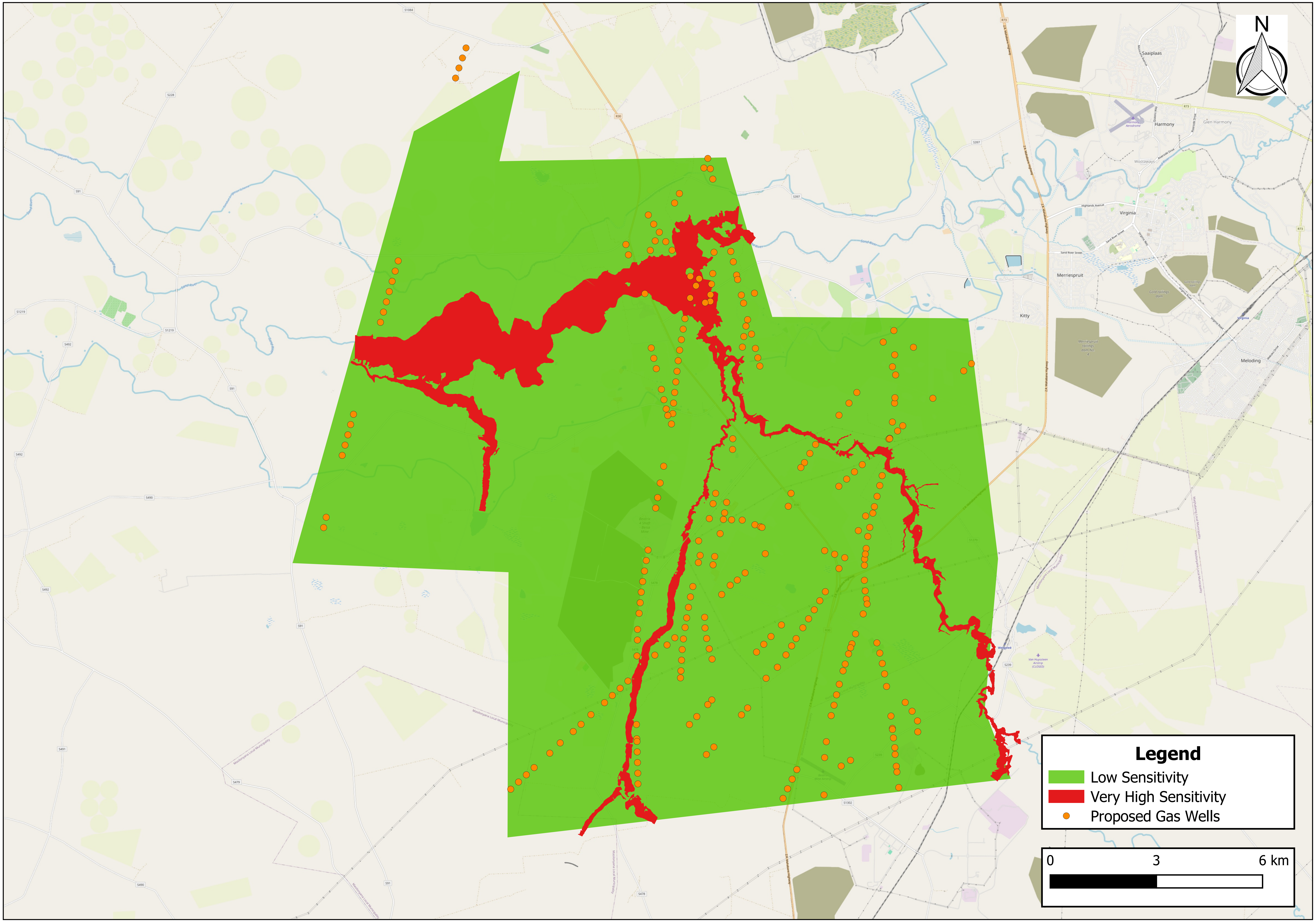
IMPACT DESCRIPTION			Post Mitigation						
Identifier	Impact	Phase	Nature	Extent	Duration	Magnitude	Reversibility	Probability	Post-mitigation ER
10.1.1	Loss of watercourse vegetation	Construction	-1	2	1	1	2	1	-1.5
10.1.2	Erosion	Construction	-1	1	1	2	2	2	-3
10.1.3	Stormwater contamination	Construction	-1	1	1	2	2	2	-3
10.1.4	Alien and/or Invasive Vegetation	Construction	-1	2	2	1	2	1	-1.75
10.1.5	Alterations of the river banks and river bed	Construction	-1	2	2	1	2	2	-3.5
10.1.6	Erosion	Operation	-1	2	4	3	2	1	-2.75
10.1.7	Stormwater contamination	Operation	-1	2	2	1	2	2	-3.5
10.1.8	Alien and/or Invasive Vegetation	Operation	-1	2	2	1	3	2	-4
10.1.9	Erosion	Decommissioning	-1	2	3	3	2	1	-2.5
10.1.10	Stromwater contamination	Decommissioning	-1	2	2	1	2	2	-3.5
10.1.11	Alien and/or Invasive Vegetation	Decommissioning	-1	2	2	1	2	1	-1.75

IMPACT DESCRIPTION				Priority Factor Criteria			
Identifier	**Impact**	**Phase**	**Confidence**	**Cumulative Impact**	**Irreplaceable loss**	**Priority Factor**	**Final score**
10.1.1	Loss of watercourse vegetation	Construction	Low	2	1	1.13	-1.6875
10.1.2	Erosion	Construction	Low	2	1	1.13	-3.375
10.1.3	Stormwater contamination	Construction	Medium	2	1	1.13	-3.375
10.1.4	Alien and/or Invasive Vegetation	Construction	Low	2	1	1.13	-1.96875
10.1.5	Alterations of the river banks and river bed	Construction	Medium	2	2	1.25	-4.375
10.1.6	Erosion	Operation	Low	2	2	1.25	-3.4375
10.1.7	Stormwater contamination	Operation	Medium	2	2	1.25	-4.375
10.1.8	Alien and/or Invasive Vegetation	Operation	Medium	2	2	1.25	-5
10.1.9	Erosion	Decommissioning	Low	2	2	1.25	-3.125
10.1.10	Stromwater contamination	Decommissioning	Medium	2	2	1.25	-4.375
10.1.11	Alien and/or Invasive Vegetation	Decommissioning	Low	2	1	1.13	-1.96875

Appendix C: Maps



N
Legend
Site Boundary
Flow Direction
1:100 Year Floodline (including climate change projection)
1:100 Year Floodline (excluding climate change projection)
Proposed Gas Wells
Pipelines
Compressor Stations
Roads
0
3
6 km


N
Legend
Low Sensitivity
Very High Sensitivity
Proposed Gas Wells
0
3
6 km
Saaiplaas
Harmony
Glen Harmony
Virginia
Merriespruit
Kitty
Meloding

Appendix D: NEMA Reporting Requirements Checklist

Reporting requirements as per NEMA Appendix 6 for specialist reports. Requirements of Appendix 6 – GN R326 EIA Regulations of 7 April 2017	Relevant section in report	Comment where not applicable
1.(1) (a) (i) Details of the specialist who prepared the report	Page i of Report – Contact details and company	-
(ii) The expertise of that person to compile a specialist report including a curriculum vita	Page iii – refer to Appendix E	-
(b) A declaration that the person is independent in a form as may be specified by the competent authority	Page ii of the report	-
(c) An indication of the scope of, and the purpose for which, the report was prepared	Section 1	-
(cA) An indication of the quality and age of base data used for the specialist report	Section 5.3	-
(cB) a description of existing impacts on the site, cumulative impacts of the proposed development and levels of acceptable change;	Section 8	-
(d) The duration, date and season of the site investigation and the relevance of the season to the outcome of the assessment	Section 6.2	-
(e) a description of the methodology adopted in preparing the report or carrying out the specialised process inclusive of equipment and modelling used	Section 5 and 6	-
(f) details of an assessment of the specific identified sensitivity of the site related to the proposed activity or activities and its associated structures and infrastructure, inclusive of a site plan identifying site alternatives;	Sections 7	-
(g) An identification of any areas to be avoided, including buffers	Section 7	-
(h) A map superimposing the activity including the associated structures and infrastructure on the environmental sensitivities of the site including areas to be avoided, including buffers;	Section 6.3	-
(i) A description of any assumptions made and any uncertainties or gaps in knowledge;	Section 6.2	-
(j) A description of the findings and potential implications of such findings on the impact of the proposed activity, including identified alternatives, on the environment	Sections 6.3, 7, 8	-
(k) Any mitigation measures for inclusion in the EMPr	Sections 8	-
(l) Any conditions for inclusion in the environmental authorisation	Sections 8	-
(m) Any monitoring requirements for inclusion in the EMPr or environmental authorisation	Sections 8	-
(n)(i) A reasoned opinion as to whether the proposed activity, activities or portions thereof should be authorised and	Section 8	-
(n)(iA) A reasoned opinion regarding the acceptability of the proposed activity or activities; and		-
(n)(ii) If the opinion is that the proposed activity, activities or portions thereof should be authorised, any avoidance, management and mitigation measures that should be included in the EMPr, and where applicable, the closure plan	Sections 8	-
(o) A description of any consultation process that was undertaken during the course of carrying out the study	-	Not applicable. A public consultation process will be handled as part of the environmental process.
(p) A summary and copies if any comments that were received during any consultation process	-	Not applicable. To date no comments regarding

		Stormwater that require input from a specialist have been raised.
(q) Any other information requested by the competent authority.		Not applicable.
(2) Where a government notice by the Minister provides for any protocol or minimum information requirement to be applied to a specialist report, the requirements as indicated in such notice will apply.	NEMA Appendix 6 and GN648 SAHRA guidelines.	

Appendix E: CVs

Neil Meyer

Technical Principal: Water Infrastructure

SMEC South Africa
Member of the Surbana Jurong Group

Personal information
- ID no.: 760810 5061 082
- South African

Years of Industry Experience
- 20+ years

Countries of Experience
- South Africa
- Rwanda
- Zambia
- Gabon
- Malawi
- Sierra Leone
- Saudi Arabia
- Lesotho

Qualifications and Memberships
- University of London, Imperial College for Science, Technology and Medicine UK, MSc HEM (Hydrology for Environmental Management), 01/11/2001
- Master of Science Engineering (cum laude) (Civil), University of Stellenbosch 08/12/2000
- Bachelor of Engineering (cum laude) (Civil), University of Stellenbosch, 02/12/1998
- Professional Engineer (Pr. Eng), Engineering Council of South Africa (ECSA), 20060199, 14/08/2006
- Member: South African Institution of Civil Engineering (SAICE), Member, 980108, 15/01/2010
- Professional: Institute of Municipal Engineering of South Africa (IMESA) No M3362 10/02/2010
- South African National Commission on Large Dams (SANCOLD)

Key Skills and Competencies
- Project Management
- Master Planning
- Hydraulic Design
- Hydrological Analysis
- Basic WTW Design
- Basic WWTW Design

Professional Overview

Neil joined SMEC South Africa in 2013.

He has 20 years' experience in the design and project management of various projects both in South Africa and internationally, plus the design and project management of bulk water, sanitation/wastewater and drainage/stormwater infrastructure including water and wastewater treatment projects.

Neil is proficient with the use of numerous software packages for the planning, design and implementation of water, wastewater and stormwater projects. Neil has also developed spreadsheet models used to simplify and optimize water, sanitation and stormwater/drainage calculations, master planning assessments and evaluations of various infrastructure and treatment related projects.

Neil completed his MSc. Eng at the University of Stellenbosch from 2000 to 2001 and his MSc. Eng HEM/DIC at the University of London, United Kingdom from 2001 to 2002.

Relevant Project Experience

C1859 | Temporary Works on High-Speed Rail Network 2 (HS2), United Kingdom | GBP +500 Billion

Client: Sub-consultant to Robert Bird Group (RBG), United Kingdom on behalf of Effage, Kier, Ferrovial Construction and BAM Nuttal (EKFB), United Kingdom

Client Contact Details: Lisa Rapson; Director, Robert Bird Group; Tel: +44 20 7633 2880; Email: lisa.rapson@robertbird.com

Description: The temporary works contractor, EKFB, was appointed to conduct Temporary Works along the future High Speed 2 Rail Network (HS2) between London and Birmingham. The temporary works consist of Civil, Structural and Road works. RBG appointed SMEC to assist with Civil designs for the temporary works. To date a total of ten (10) earthwork design packages have been delivered.

Role and Responsibilities: Design lead for stormwater design and innovative drainage solutions for various excavations for temporary works. Design involvement included stormwater collection, routing, attenuation, silt management and pumping of stormwater. Hydraulic modelling of attenuation structures prepared using EPASWMM.

C1881 - Ernest Robertson Dam Dam Safety Evaluation, Western Cape, South Africa | R 92,366 Fees

Client: Mossel Bay Local Municipality | **Dates:** April 2022 – June 2022

Client Contact Details: Catherine Koelman; Project Manager; +27 (0)44 606 5269

Description: The 5th dam Safety Evaluation (DSE) for the Ernest Robertson Dam was undertaken in 2013. The 6th DSE was due, as required by the Department of Water and Sanitation (DWS) in terms of Regulations 35 of the Regulations regarding safety of dams published in government notice R.139 dated February 2012. SMEC was tasked with undertaking the 6th DSE. The scope of services of the Dam Safety Evaluation were as follows:

- Dam Inspection: Undertake the dam safety inspection and state the condition of indicators including the dam wall, dam crest and spillway, outlet works, reservoir basin slopes and monitoring instruments.
- Evaluation and Reporting: Review dam monitoring data to identify any issues; confirm flood hydrology and spillway capacity values remain applicable; prepare and submit draft Dam Safety

Evaluation Report with recommendations and action plan; Update and submit final Dam Safety Evaluation Report following receipt of comments from the client.

Role: Technical Lead.

Responsibilities: Review of Flood hydrology calculations, spillway capacity calculations, and report.

JH0049 - Tetra4 Gas Floodlines, Free State, South Africa | R 348 000 Fees

Client: EIMS | **Dates:** January 2022 – Ongoing

Client Contact Details: Brian Whitfield; Project Manager; +27 (0)82 688 9850

Description: SMEC was engaged by EIMS to prepare a Hydrological Impact Assessment that will be required to assist with the application of a Water Use License and Environmental Authorization for the Tetra4 Gas Production Project located in Welkom, Free State province.

Several hydrological methods, including Rational Method, Alternative Rational Method and SDF method were considered to calculate peak flood discharges for various return periods.

River hydraulics were modelled using the GeoHECRAS software suite developed by CivilGEO Engineering Software. The geometric information for the model was obtained from local topographic survey and roughness coefficients estimated from site surveys, based on the HEC-RAS hydraulic reference manual descriptions.

A flood hazard map and hydrological study report was prepared as input to various regulatory approval applications.

Role: Technical Lead.

Responsibilities: Review of Hydrological Analysis, Hydraulic Analysis, and the Hydrological assessment report.

Jh0051 - Mogalakwena PV Hydrological Study, Limpopo, South Africa | R250 917 Fees

Client: EDF Renewables | **Involvement Period:** April 2022 – July 2022

Client Contact Details: Martin Zietsman; Project Manager; +27 (0)83 69 13701

Description: SMEC was engaged by EDF Renewables to prepare a Hydrological Impact Assessment for a PV plant located in the Limpopo province of South Africa. This Hydrological Impact Assessment deals with the following aspects:

- Hydrological Analysis.
- Hydraulic Modelling.
- Floodline Delineation; and
- Flood impacts on infrastructure and flood mitigation measures.

The project also involved the design of a conceptual stormwater management plan. The scope of work was the design of a drainage layout, the sizing of drainage channels and detention basins, and erosion protection measures.

Role: Project manager and Design Engineer.

Responsibilities: Review of Hydrological Analysis, Hydraulic Analysis, Hydrology report and the stormwater management plan.

JH0050 - UMSO PV Hydrological Study, Northern Cape, South Africa | R 276 766 Fees

Client: EDF Renewables | **Dates:** January 2022 - Ongoing

Client Contact Details: Bradley Rabbitte; Project Manager; +27 (0)72 855 3420

Description: SMEC was engaged by EDF Renewables to prepare a Hydrological Impact Assessment for 5 PV plants located in the Northern Cape province of South Africa. This Hydrological Impact Assessment deals with the following aspects:

- Hydrological Analysis.
- Hydraulic Modelling.
- Floodline Delineation; and
- Flood impacts on infrastructure and flood mitigation measures.

Role: Technical Lead.

Responsibilities: Review of Hydrological Analysis, Hydraulic Analysis, and the Hydrology report.

DM0226: Replacement of AC/Mains for eThekwini Water and Sanitation, Phase II, Durban, KwaZulu-Natal, South Africa | R200 million

Client: eThekwini Municipality | Date: 2022 – Ongoing

Client Contact Details: Devashan Govender; Project Manager; Contact details: devashan.govender@durban.gov.za

Description: Replacement project comprising 12 months of intense field work and analysis to identify and select critical reservoir zones based on multi parameter optimization algorithms using GIS tools as part of the EWS water master plan and asset replacement programme for 2015/2030. A total of 80km of water mains to be designed already identified under phase I of the project. Prepare specification and tender documents for 40km of water mains in eThekwini Water Supply area.

Role and Responsibilities: Project Engineer, Lead Design Engineer. Technical advisor to field and data analysis teams in developing strategies to prioritize critical reservoir zones based on key KPI's. Lead the design work, prepare tender documentation, specification and project coordination of 2 construction contracts.

XL0048: NEOM Trojena, Stages 3B,3C,3D - Saudi Arabia | R 25 million (fees)

Client: Surbana Jurong (SJ) | **Date**: March 2022 – Ongoing

Contact Details: Sybille Tildsley - sybille.tildsley@smec.com

Description: SMEC International signed a sub-consultant agreement with Surbana Jurong (Holding Company) for the design of a futuristic city and freshwater lake in the NEOM mountains of Saudi Arabia. The project comprises all disciplines of stormwater, water, foul water, irrigation, recycled water and all the associated treatment processes. The harsh terrain required the teams to develop innovative solutions to provide wet services while managing the water quality of an artificial lake with challenges of high evaporation, lake seepage through designed liners etc. The project comprised confirming the master planning, developing the concept design through detailed design to tender and construction supervision.

Role and Responsibilities: Water Design Expert. Responsible for design development of bulk water systems for lake filling, lake recirculation and lake water treatment. Coordinating technical input required from potable water, foul water, recycled water, and treated water systems to ensure Lake water levels and quality is ensured through the correct sizing and placement of associated wet utility services around the lake and within the site-wide mountain assets as planned. Responsible to coordinate the design of stormwater and stormwater treatment systems impacting the Lake Water Quality.

Ferreira Canal, ESwatini | USD 27,000 (fees)

Client: eSwatini Electricity Company | **Date**: January to March 2022

Client Contact Details: Charles Coleman, Power Stations Manager, +268 550 2611, charles.coleman@sec.co.sz

Description: The Edwaleni Hydropower Station receives water from the Little Usutu and the Great Usutu rivers via two canals; the Main Canal and the Ferreira Canal respectively. This project entails the design of improvements to the Ferreira Canal (approximately 7.2 km in length and predominantly unlined) to increase the flow capacity to 6m^3/s, by enlarging and lining.

Role and Responsibilities: Technical Hydraulic Design Support and Peer Review. Review hydraulic models, advise on sizing/position of sediment traps, junction boxes/stilling basins and inlet/outlet structures. High level input to quantities and cost to preliminary design levels, input with regards to constructability to the Preliminary Design Report.

C1847: Juba-Rumbek Road Upgrade – Hydrological Study Review, South Sudan | R 0.1 million (fees)

Client: SMEC International | **Date**: Jan 2021 – March 2021

Client Contact Details: Daniel Kamau Daniel.Kamau@smec.com +254 20 444 1541/2/3

Description: The upgrade of the 63 km road from Juba to Rumbek in South-Sudan has been prioritized by the Ministry of Roads and Transport to address severe flooding. The project comprises the upgrading of at least 5 large bridges and up to 60 culverts along the route for which flood modelling and hydraulic capacity calculations were reviewed.

Role and Responsibilities: Specialist Hydrologist / Hydraulic Engineer. Responsible for review of hydrological calculations of the 1:50 and 1:100-year events, including hydraulic capacity reviews of structures.

XL0022: Consulting Engineering Services for the Upgrading of the Mpiti to Sehlaba Thebe Road Project – Hydrological Study Review, Lesotho | R 0.1 million

Client: Ministry of Public Works & Transport, Lesotho| **Date**: Nov 2020 - 2021

Client Contact Details: SA Thamae: +266 22 324191

Description: Hydraulic capacity reviews of 20 key culverts along the 90 km length of road, including full hydrological modelling of mountain catchments using various flood estimation methods. Advising on culvert upgrades.

Role and Responsibilities: Specialist Hydrologist / Hydraulic Engineer. Responsible for review of hydrological calculations of the 1:20 and 1:50 year events including hydraulic capacity reviews of existing structures.

XL0048: Neom Mountain Lake and Village, Stage 3A - Saudi Arabia | R 13 million (fees)

Client: Bureu Proberts | **Date**: Oct 2020 – June 2021

Contact Details: skyer@bureauproberts.com.au

Description: SMEC International signed a Contract with an international architect (name undisclosed – under NDA) who won a design competition for the design of a Lake and Lake village located within mountain resort project. SMEC South Africa is required to provide input to the Feasibility and Concept Design for various Infrastructure, Dam, Geology, Hydrology, Power & Urban Infrastructure of the Lake and Village.

Role and Responsibilities: Water Engineer / Stormwater Engineer. Responsible for undertaking Lake water balances, determining bulk water requirements, lake filling times, lake management energy requirements and costs, lake catchment stormwater conceptual designs, flood calculations and development and sizing of stormwater treatment options. Conceptualizing and sizing and Desalination of Lake Water and management of brine.

XL0049: Consultancy Services for Freetown Water Supply and Sanitation Master Plan and Medium-Term Investment Project Proposal. GVWC, Freetown, Sierra Leone | R5.67 million (fees)

Client: Guma Valley Water Company – Sub-Consultant to COBA, Portugal| **Date**: 2020 - Ongoing

Client Contact Details: Francis H Lahai PE MSLIE, Contact Nr. +232 78781396, Contact Nr. ++232 30642872; Julio Arsenio (COBA); Contact Nr: +351 210 125 000

Description: The project addresses the water and sanitation master planning for Freetown with a population of 1.5 million people where dilapidated water and infrastructure forced authorities to plan ahead for the identification of short, medium- and long-term investment projects.

Role and Responsibilities: External Water & Sanitation Master Plan Reviewer. Responsible to direct and review inputs from a team with Sanitary Expert, Drainage Expert, Water Resources Expert, Financial Expert, Groundwater Expert and RAP/Environmental Expert. Directing master planning and design related philosophies, approaches and guidelines.

DM0020: Review of the Ndumo A Irrigation Scheme, Jozini, South Africa | R 0.5 million (fees)

Client: Department of Treasury, KwaZulu-Natal, South Africa | | **Date:** 2020

Client Contact Details: Nolwazi Maduma/ Rob Kempen, Project Managers, Contact Nr. +27 33 897 4496 / +27 82 651 3898; Nolwazi.Maduma@kzntreasury.gov.za / Rob.Kempen@kzntreasury.gov.za

Description: The project aimed to identify various alternative pumping main routes from the Pongola and other rivers to service the Ndumo A Irrigation Scheme more effectively and sustainability. The project concluded deficiencies in the original design and assisted the client to make informed discussion to rectify and approve the pumping system to ensure a sustainable overall scheme.

Role and Responsibilities: Hydraulic Modelling Expert. Responsible for the review of existing river abstraction works on the Pongola River and rising mains, storage reservoir hydraulic modelling as well as option development and hydraulic modelling for alternative irrigation bulk water supply options to the Ndumo A Irrigation Scheme. Development of review comments, reporting to the Project Manager.

XL0037: Master Plan of Proposed Airport City in Nkok, Gabonese Republic | R2.1 million

Client: DP Architects PTE LTD, Singapore | **Date:** 2018 - 2019

Client Contact Details: Djoko Prihanto, Project Manager, Contact Nr. + +65 6338 3988 & Dave Duke; +27 31 277 6600 dparchitects@dpa.com.sg

Description: Stormwater and flood modelling for Airport City with primary focus to confirm 1:50 and 1:100-year drainage lines to guide Town Planning process to ensure most suitable and efficient positioning of roads, stands and major infrastructure.

Role and Responsibilities: Hydrologist. Technical advisor on rainfall and runoff generation and stormwater/flood modelling using HEC-RAS 2D software. Services provided to SMEC South African team developing overall master plan for Airport City.

DH874: Investigations in the Improvements for Autumn Drive Dam, Umhlanga as Multipurpose Facility, KwaZulu-Natal, South Africa | R0.065 million

Client: Tongaat Hulett Developments | **Date:** 2016 - 2018

Client Contact Details: Lawrence Kirkman; PM; Contact Nr. +27 31 560 1900

Description: Hydrological & Hydraulic modelling of stormwater systems, dam and spillway to optimize re-use potential of dam considering both applications for retention and aesthetics.

Role and Responsibilities: Project Director. Liaise with client's representative, oversee modelling work in PCSWMM and review technical reports.

DT0001: Flood Calculations for Farm Dam SANRAL N1-17 at km 13.600, KwaZulu-Natal, South Africa

Client: SANRAL | **Date:** 2018

Client Contact Details: Zandile Nene; PM; Contact Nr. +27 33 392 8139

Description: Culvert hydraulics and river flood level modelling

Role and Responsibilities: Hydraulics Engineer. The Hydraulic Engineer undertook flood calculations for a river section at SANRAL's N1 Bridge at chainage 13.6km to ascertain a suitable flood outlet level for a farm dam downstream of the N1 Bridge to evaluate back-water effects on the N1 river bridge.

PE243: Heuningness Estuary, Western Cape Province, South Africa | R0.4 million

Client: Western Cape Nature Conservation | **Date:** 2016 - 2017

Client Contact Details: Pierre de Villiers; Programme Manager; Contact Nr. +27 21 866 8000 estuaries@capenature.co.za

Description: Undertake hydrological and hydrodynamic modelling to predict water (flood) levels under feasible system and mouth management scenarios for a big an area as possible of the Heuningnes Estuary and catchment. Provide recommendations and substantiated motivations for a mouth management regime/s that best balances ecological and human needs for the foreseeable future.

Role and Responsibilities: Project Manager. Project management and technical assistance to flood modelling, flood peak arrival

DH874: Investigations in the Improvements for Autumn Drive Dam, Umhlanga as Multipurpose Facility, Durban, KwaZulu-Natal, South Africa | R0.065 million

Client: Tongaat Hulett Developments | **Date:** 2016

Client Contact Details: Lawrence Kirkman; PM; Contact Nr. +27 31 560 1900

Description: Hydrological & Hydraulic modelling of stormwater systems, dam and spillway to optimize re-use potential of dam considering both applications of retention and aesthetics.

Role and Responsibilities: Project Director. Liaise with client's representative, oversee modelling work in PCSWMM and review technical reports.

DM0113: Cwaka Environmental Impact Assessment and Formalization, KwaZulu-Natal, South Africa | R1 million

Client: LDM Consulting | **Date:** 2016

Client Contact Details: Trivi Arjunan; PM; Contact Nr. +27 31 207 1340

Description: Floodline delineation and report.

Role and Responsibilities: Design Engineer, Hydraulic modelling Oversight. Hydraulic modelling and floodline delineation of 100-year floodlines for two major rivers in the Cwaka area using HEC-RAS software, drafting and reporting

DM0120: Rukwa Coal Project – Flood Analysis, Rukwa, Tanzania | R0.3 million

Client: Shangoni Management Services | **Date:** 2016

Client Contact Details: Dawie Maree, Contact Nr. +27 73 330 5815

Description: Hydrological flood modelling with UPFD software and hydraulic routing and mapping with HEC-RAS.

Role and Responsibilities: Project Manager. Oversee and project management of floodline and flood volume assessment for three major rivers for Rukwa Coal Mine.

PK270: Polokwane Wastewater Treatment Works Flood Line Analysis, Polokwane, South Africa | R 8 million

Client: Polokwane Municipality | **Date:** 2017

Client Contact Details: Vonani Mathebula, Director, Contact Nr. 072 153 3175

Description: Flood line delineation and report for the construction of a new wastewater treatment works.

Role and Responsibilities: Hydraulic Modelling Reviewer. Oversee hydrological study for two rivers' catchments (the Bloed River and the Sand Riviera) for the purposes of delineating the 1:20, 1:50 and 1:100-year floods. Review hydraulic modelling of the rivers for delineation of flood lines for the various storm events using HEC-RAS modelling software. The results were reported for the purposes of positioning the wastewater treatment works appropriately.

DD0081: Upgrade of KwaNqetho Inlet 300mm Ø Steel Pipe Watermain, Durban, KwaZulu-Natal, South Africa | R 10 million

Client: eThekwini Water and Sanitation | **Date:** 2016

Client Contact Details: Devashan Govender PM (Leisel Bowes); Contact Nr. +27 31 311 8796

Description: In the execution of eThekwini's water master plan and wider drive for asset renewal, the project considered the investigation and pipe replacement of a problematic section of water main in a challenging (steep topography) with a high historic frequency of bursts.

Role and Responsibilities: Lead Hydraulic Modeller, Design Review, Technical Advisor. Hydraulic modelling of existing water distribution system to determine cause of failure using Bentley WaterGEMS hydraulic modelling software, analysing pressure and flow data, modelling of proposed system with new connectivity to optimise break-pressure tank positions, design of proposed upgrade (diameters). Provide technical advice and design review to EWS on related matters such as valve selection, erosion protection and connectivity.

DD451 Developing a Stormwater Flood Risk Assessment Tool, Phoenix, KwaZulu-Natal, South Africa | R60k

Client: eThekwini Municipality, Coastal Stormwater & Catchment Management | **Date:** Jan 2015 – Feb 2015

Client Contact Details: Kiyash CherrSha, Contact Nr. 031 311 7323

Description: Pilot study to develop a storm water flood risk assessment tool. The assignment involved hydrological and hydraulic modelling (using PCSWMM software) of an urban catchment in Phoenix to the north-west of Durban comprising 479 sub-catchments, 18,400m of storm water pipes with diameters ranging from 225mm to 2,000mm.

Role and Responsibilities: Project Manager. Oversee and project management, Review of hydrological and hydraulic modelling. PCSWMM software.

DM0089: Pre-Feasibility Investigation, Water, Sewage & Effluent requirements, HEBEI Iron & Steel Industry, Richards Bay, KwaZulu-Natal, South Africa | R 1.3 billion

Client: Richards Bay Infrastructure Development Zone (IDZ) | **Date:** 2015

Client Contact Details: Brenda Mabaso; Research, Marketing Intelligence Manager; Contact Nr. +27 35 788 0571

Description: Feasibility studies, water & sewer services for planned Steel Smelter in Richards Bay.

Role and Responsibilities: Design Engineer / Support to Project Manager. Prepare high level feasibility studies on bulk water and sanitation supply for planned Steel Smelter in Richards Bay, analysis included various technical options and costs comparison's to ultimately inform decision makers on investment options and key timeframes.

DM0035: DUT Riverside and Indumiso Campus Storm Water Management Plan (Planning), Pietermaritzburg, KwaZulu-Natal Province, South Africa | R1.2 million

Client: Durban University of Technology | **Date:** Aug 2013 – Feb 2017

Client Contact Details: Tom McKune, Contact Nr. +27 (0)86 010 3194

Description: Civil and structural engineering services for the infrastructure upgrade at the Riverside campus of DUT in Pietermaritzburg. New engineering building, lecture halls, library and computer centre. Determination and delineation of 1:50 and 1:100 flood lines for the Msunduzi River at the Durban University of Technology (DUT) Riverside Campus.

Role and Responsibilities: Hydrological/Hydraulic Engineer. Hydrological calculations and Hydraulic Modelling of the Msunduzi River for delineation of 1:50 and 1:100-year flood lines including sensitivity analysis of building structures in the 1:100-year floodplain.

Rehabilitation of Centurion Lake, Pretoria, South Africa | R10 million

Client: City of Tshwane, Roads & Stormwater | **Date:** 2013

Client Contact Details: Gawie Janse van Vuuren; PM; Contact Nr. +27 21 358 9999

Description: Hydraulic capacity calculations.

Role and Responsibilities: Design Engineer. Project management and coordination of specialist river rehabilitation and flood hydrology studies. Hydraulic optimization of proposed drainage and diversion structures in support of the rehabilitation of the Centurion Lake suffering from toxic sedimentation pollution. Hydraulic investigations were undertaken for the Hennops River which included the SANRAL N1 road bridge section in Centurion. HEC-RAS software was used following hydrological inputs from XP-SWMM software.

Flood overtopping of N11 between Amersfoort and Ermelo, Mpumalanga, South Africa | part of R350 million project

Client: South African National Roads Agency | **Date:** 2008 - 2011

Client Contact Details: Willem van der Merwe, Contact Nr: +27 12 426 6200

Description: Hydraulic capacity calculations.

Role and Responsibilities: Hydraulics Engineer. The Hydraulic Engineer working for SCIP Engineering Group undertook flood calculations following flooding of a section of the N11 which involved hydrological calculations and culvert capacity assessments based on photo evidence and high-water levels observed during the flood event.

Professional History

- **2013 – Present | SMEC South Africa**
  2013 – Present | Technical Principal, Water Infrastructure
- **2003 – 2013 | SCIP Engineering Group (Pty) Ltd, Witbank**
  2003 – 2013 | Director
- **2001 – 2003 | Group 5 Roads & Earthworks (Pty) Ltd**
  2001 – 2003 | Site Agent
- **2000 – 2001 | Post graduate studies, University of London**
  2000 – 2001 | Student
- **1998 – 2000 | Post Graduate studies, Sigma Beta/Water Resources Commission, University of Stellenbosch**
  1998 – 2000 | Student

Courses and Conferences Attended

2020	IMESA	Site visit to 20 MLD Rosetta Water Treatment Works
2019	University of Cape Town	Permeable Pavements and Bio Retention Cells
2019	WISA	Getting Control Valves Right
2017	WISA	Energy recovery in pipelines – micro turbines
2016	WRC, University of Pretoria	Biofilm n water mains
2016	WISA	Water Institute South Africa – 2016 Conference
2015	University of Cape Town	Report Writing
2015	University of Cape Town	Sustainable Drainage Systems (SuDS)
2014	WISA	CFD & Pipe/Earth interaction
2014	Wolf Weidemann Pr Eng.	Finances for Built Environment Profession
2013	WISA Conference	Annual Conference
2013	University of Pretoria/SINOTECH	Conduit Hydropower
2013	Kaytech	Filtration & pipe material

Publications and Papers Presented

2000	MSc Thesis on Flood Measurement Techniques using Bridge Structures – University of Stellenbosch
2001	MSc HEM Thesis on Groundwater Recharge to Coastal Plains, Aden/Southern Yemen – University of London

Language Skills

Mother Tongue:	Afrikaans		
Languages	**Speak**	**Read**	**Write**
English	Excellent	Excellent	Excellent
Afrikaans	Excellent	Excellent	Excellent

Rendani Byven Thovhakale

Water Engineer

Years of Industry Experience

- 6 years

Personal Information

- Cell Number: +27 78 041 1701
- Email: rendanitb@yahoo.com
- Nationality: South African

Qualifications

- Bachelor of Engineering (Civil), University of Johannesburg, 2015

Key Skills and Competencies

- Hydrological analysis
- River hydraulics modelling
- Floodline delineation
- Surface Drainage
- Pipeline and Pump station design
- Erosion protection structures
- Energy dissipation structures
- Stormwater ponds
- AutoCAD Civil 3D
- AutoCAD
- GeoHEC-RAS
- QGIS
- Microsoft Excel

Professional History

- 2019 – Present | Engineer
- 2016 – 2019 | Graduate Engineer

Referees

Dawid van Coller, Senior Water Engineer, vancollerd@gmail.com, +44 7748 176 086

Roshuma Makhado, Classmate, roshumamakhado@gmailcom, +27 79 251 9246

Professional Overview

Rendani is a Water Engineer with 6 years of experience in the civil engineering industry, during which time he has developed varied technical expertise, primarily in the water sector. He is highly proficient in Hydrology and River hydraulic modelling and related studies having completed numerous hydrological and floodline studies on several international projects, most notably for the Lesotho Highlands Water project. Often the design of erosion protection measures or river rehabilitation work also form part of these projects. My expertise also extends to the detailed design of hydraulic components associated with river systems such as weirs, canals, and erosion protection structures.

Some of the projects he has been involved in include the feasibility design and planning of steel and concrete pipelines and pump stations.

Relevant Project Experience

Ernest Robertson Dam DSE, Western Cape, South Africa | US$ 5 621

Client: Mossel Bay Local Municipality | **Dates:** April 2022 – June 2022

Client Contact Details: Catherine Koelman; Project Manager; +27 (0)44 606 5269

Description: The 5th dam Safety Evaluation (DSE) for the Ernest Robertson Dam was undertaken in 2013. The 6th DSE was due, as required by the Department of Water and Sanitation (DWS) in terms of Regulations 35 of the Regulations regarding safety of dams published in government notice R.139 dated February 2012. SMEC was tasked with undertaking the 6th DSE. The scope of services of the Dam Safety Evaluation were as follows:

Dam Inspection: Undertake the dam safety inspection and state the condition of indicators including the dam wall, dam crest and spillway, outlet works, reservoir basin slopes and monitoring instruments.

Evaluation and Reporting: Review dam monitoring data to identify any issues; confirm flood hydrology and spillway capacity values remain applicable; prepare and submit draft Dam Safety Evaluation Report with recommendations and action plan; Update and submit final Dam Safety Evaluation Report following receipt of comments from the client.

Role: Design Engineer.

Responsibilities: Flood hydrology calculations, checking of spillway capacity, and preparation of report.

Tetra4 Gas Floodlines, Free State, South Africa | US$ 21 178 Fees

Client: EIMS | **Dates:** January 2022 – Ongoing

Client Contact Details: Brian Whitfield; Project Manager; Ph +27 (0)82 688 9850

Description: SMEC was engaged by EIMS to prepare a Hydrological Impact Assessment that will be required to assist with the application of a Water Use License and Environmental Authorization for the Tetra4 Gas Production Project located in Welkom, Free State province.

Several hydrological methods, including Rational Method, Alternative Rational Method and SDF method were considered to calculate peak flood discharges for various return periods.

River hydraulics were modelled using the GeoHECRAS software suite developed by CivilGEO Engineering Software. The geometric information for the model was obtained from local topographic survey and roughness coefficients estimated from site surveys, based on the HEC-RAS hydraulic reference manual descriptions.

A flood hazard map and hydrological study report was prepared as input to various regulatory approval applications.

Role: Project manager and Design Engineer.

Responsibilities: Review of Hydrological Analysis, Review Hydraulic Analysis, Floodline delineation and preparing the Hydrological assessment report.

Rendani Byven Thovhakale

Water Engineer

Mogalakwena PV Hydrological Study, Limpopo, South Africa | US$ 15 270

Client: EDF Renewables | **Involvement Period:** April 2022 – July 2022

Client Contact Details: Martin Zietsman; Project Manager; Ph +27 (0)83 691 3701

Description: SMEC was engaged by EDF Renewables to prepare a Hydrological Impact Assessment for a PV plant located in the Limpopo province of South Africa. This Hydrological Impact Assessment deals with the following aspects:

- Hydrological Analysis;
- Hydraulic Modelling;
- Floodline Delineation; and
- Flood impacts on infrastructure and flood mitigation measures.

The project also involved the design of a conceptual stormwater management plan. The scope of work was the design of a drainage layout, the sizing of drainage channels and detention basins, and erosion protection measures.

Role: Project manager and Design Engineer.

Responsibilities: Review of Hydrological Analysis, Hydraulic Analysis, Floodline delineation and preparing the Hydrology report. Design of stormwater management plan.

UMSO PV Hydrological Study, Northern Cape, South Africa | US$ 16 843 Fees

Client: EDF Renewables | **Dates:** January 2022 - Ongoing

Client Contact Details: Bradley Rabbitte; Project Manager; Ph +27 (0)72 855 3420

Description: SMEC was engaged by EDF Renewables to prepare a Hydrological Impact Assessment for 5 PV plants located in the Northern Cape province of South Africa. This Hydrological Impact Assessment deals with the following aspects:

- Hydrological Analysis;
- Hydraulic Modelling;
- Floodline Delineation; and
- Flood impacts on infrastructure and flood mitigation measures.

Role: Project manager and Design Engineer.

Responsibilities: Review of Hydrological Analysis, Hydraulic Analysis, Floodline delineation and preparing the Hydrology report.

Kaalspruit Climate Resilient Catchment Management Plan, Gauteng Province, South Africa | US$ 105 246 Fees

Client: Gauteng Department of Agriculture and Rural Development (GDARD) | **Dates:** August 2021 - Ongoing

Client Contact Details: Gerson Nethavhani; Project Manager; Ph +27 (0)11 240 3435

Description: The assignment entailed the development of a climate-resilient Catchment Management Plan (CMP) for the Kaalspruit catchment to the east of Johannesburg. The 1st step in developing the CMP was to identify the diverse stakeholders in the catchment and to prepare a Stakeholder Engagement Plan. This was followed by stakeholder engagement and literature review leading to a description of the catchment status quo in the form of a Situational Assessment Report. This step included development of a base case hydrological and hydraulic model using PCSWMM software. Planned future steps were identification of potential catchment interventions and testing of these in the model to assess physical benefits, further stakeholder engagement, and ultimately the development of the CMP.

Role: Project Manager and Design Engineer

Responsibility: Hydrological and Hydraulic analysis.

Calitzdorp Spa Dam, Northern Cape Province, South Africa | US$ 7647 Fees

Client: Calitzdorp Export Agri Hub | **Dates:** April 2021 - July 2021

Client Contact Details: Gerhard Meyer; Project Manager; Ph +27 (0)82 802 7138

Description: Execution of a Water Resource Study to investigate the feasibility of the proposed Calitzdorp Spa Dam. The primary purpose of the Study was to ascertain whether there is sufficient water available in the catchment over the long-term for the intended water use, at a sufficiently high assurance of supply. Four potential dam sites were assessed using the Water Resources Simulation Model (WRSM/Pitman), taking environmental water requirements into account. The Study had a positive outcome, and the following investigations were scoped for execution subject to funding availability.

Role: Design Engineer

Responsibility: Water resources modelling

Pandora Water Extraction, North West Province, South Africa | US$ 41 000 Fees

Client: Eastern Platinum Limited | **Dates:** November 2020- April 2021

Client Contact Details: Andre Laubscher; Project Manager; Ph +27 (0)82 228 7069

Description: To supplement water supply to the Marikana Platinum Mine, Sibanye Stillwater have secured an allocation from the Hartbeestpoort Dam Irrigation System. The project will entail the detail design of the following components: Extraction point from the West Canal Hartbeespoort Dam Irrigation System; gravity feed pipeline/canal from the offtake to a new holding dam with a transfer capacity of 10 million litres per day; 30 million litre (3 days) holding dam adjacent to the irrigation canal; and pump station fed from the holding dam and delivering into an existing 315mm diameter pipeline which is connected to the mine's water reticulation/distribution system.

Role: Design Engineer

Responsibility: Preliminary design of Pump Station and 5.3km HDPE pipeline

Mokopane Treated Wastewater Pipeline, Limpopo, South Africa | US$ 91 500

Client: Anglo American Platinum | Date: August 2020 - December 2020

Client Contact Details: Chiedza Mnguni; Project Manager; Chiedza.mnguni@angoamerican.com

Anglo American Platinum intends to improve the current 30km long, 250mm and 300mm diameter steel pipeline's capacity. The pipe is intended to deliver 6Ml/day which is an improvement over the 4.42Ml/day that it delivers currently in 2020. SMEC was assigned to investigate the possible options for improving the current pipe system. These options included analysing: various pipe sizes for pipe replacement; lining options for refurbishing the current pipe; required pump station capacity; and cost models for all options.

Role: Design Engineer

Analysed the capacity of the existing pump station and Pipeline; Designed options for improving the pipe system capacity; and prepared the feasibility study and cost models

Steynsrus Water Supply Scheme, Free State, South Africa | US$ 38 000

Client: MIB Infrastructure Development | Date: May 2020 - July 2020

Client Contact Details: Papi Wessie; Project Manager; Ph (+27) 12 942 4450

The existing Steynsrus Water Supply Scheme sources water from the Vals River and supplies the towns of Steynsrus and Matlwangtlwang. The scheme comprises an abstraction weir and pump station on the Vals River, which pumps raw water via a 400 mm diameter low pressure asbestos-cement (AC) pipeline into the off-channel Morgenzon Dam. Water is stored in the dam and pumped from there by a high lift pump station via a booster pump station and balancing reservoir to the water treatment works (WTW), from whence treated water is supplied to Steynsrus and Matlwangtlwang. These towns regularly suffer from water shortages. This feasibility study investigated options to augment the supply to the town. A raising of the dam in combination with an upgrade of the pump station was the recommended option.

Role: Design Engineer

Performed the Water Resource Study, Analysed the capacity of the existing pump station and Pipeline and prepared the feasibility study

Steenkoolspruit Hydrodynamic Modelling, Mpumalanga, South Africa | US$ 9 500 Fees

Client: Anglo American Coal South Africa | Date: April 2020 - May 2020

Client Contact Details: Marthinus van Wyk; Project Manager; Ph +27 (0)17 620 2714

SMEC was engaged by the Anglo American Coal South Africa to undertake a Hydrological and Flood Risk Assessment at the Isibonelo Colliery which is located 9 km to the north of Secunda, Mpumalanga Province. The objective of this study was to investigate the impacts of removing the Isibonelo Attenuation Dam on flood levels on the farmlands upstream, and on the mining area downstream. A 1D hydrodynamic HEC-RAS model was used to determine flood levels of various flood events in combination with a flood routing model to take into account the attenuation effects of the existing dam.

Role: Design Engineer

Review of Hydrological Analysis, Hydraulic Analysis, Floodline delineation and preparing the Hydrology report.

Polokwane Waste Water Treatment Works, Limpopo, South Africa | US$ 50 000 000m

Client: Mafumu Consulting (Pty) Ltd | Date: March 2020 - March 2021

Client Contact Details: Terrence Mathebula; Manager; Ph +27 72 153 3175

Development of the new Polokwane Regional Wastewater Treatment Works with an ultimate capacity of 40ML/day. The scope of SMEC's appointment entails design, documentation and procurement, construction monitoring and contract administration. The works are being implemented in two contracts, namely an earthworks contract and a main works contract.

Role: Design Engineer

Design of a 1m diameter and 100m long concrete pipe and the design of an energy dissipation structure. Design of stormwater drains. Site Supervision

Lesotho Highlands Water Project Delivery Tunnel North Maintenance Shutdown, Free State Province, South Africa | US$ 710 000

Client: Trans Caledon Tunnel Authority (TCTA) | **Date**: Oct 2019 – Feb 2020

Client Contact Details: David Keyser, Project Manager; Ph +27 12 683 1203

Description: The 4,6m diameter and 22km long Delivery Tunnel North which is part of the Lesotho Highlands Water Project was constructed in the 1990s to transfer water to the Gauteng Provence of South Africa. SMEC undertook a planned inspection of the tunnel during a 9week system outage to identify the repair and maintenance requirements. Other works that were undertaken during that period involved the inspection of the Ash River to assess erosion and deposition conditions along the river and to assess the status of existing structures along the river. SMEC procured a contractor and repairs and maintenance of tunnel lining and valves were executed, all within the outage period.

Role: Design Engineer and Inspector

Responsibilities: Inspection of the Ash River, Hydraulic modelling, preparing the Ash River Inspection report.

Isibonelo Dam Inspections, Mpumalanga Province, South Africa| US$ 6 700

Client: Anglo American Coal South Africa | **Date**: December 2019

Client Contact Details: Marthinus van Wyk, Project Manager; Ph +27 17 620 2714

Description: SMEC South Africa (SMEC) was appointed by Anglo American Coal South Africa (AACSA) to carry out an annual safety inspection for five dams at their Isibonelo Colliery including:

- Attenuation Dam (Category II 11.5m high earthfill embankment with Armco Culvert Spillway)
- Diversion Dam (Category II 10.5m high earthfill embankment with side channel and auxiliary culvert spillway)
- Farm Dam (Uncategorized approximately 5m high earthfill embankment with side channel spillway)
- Montedi Dam (Uncategorized approximately 5m high earthfill embankment with side channel spillway)
- Vaskop Dam (Category II 13.5m high earthfill embankment with side channel spillway)

The main purpose of the dam inspection was to assess the condition of each of the following indicators: Wall embankment; Inlet; Outlet; Spillway; Pump station; Leak detectors; and Safety and security.

Role: Dam Inspector

Responsibilities: Dam inspections and preparing the dam inspection reports.

Emalahleni Discard Dump Floodlines, Mpumalanga Province, South Africa| US$ 4 000

Client: Shangoni Management Services | **Date**: November 2019

Client Contact Details: Christiaan Schutte, Project Manager; Ph +27 82 784 2942

Description: SMEC was engaged by Shangoni Management Services to undertake a floodline study for the proposed discard dump in Emalahleni, Mpumalanga Province.
This study report documents the results of the floodline study which deals with the following aspects:

- Hydrological Analysis
- Hydraulic Modelling
- Flood routing
- Floodline Delineation; and

Several hydrological methods, including Rational Method, Alternative Rational Method and SDF method were considered to calculate peak flood discharges for various return periods.
River hydraulics were modelled using the GeoHECRAS software suite developed by CivilGEO Engineering Software. The geometric information for the model was obtained from local topographic survey and roughness coefficients estimated from site surveys, based on the HEC-RAS hydraulic reference manual descriptions.

A floodline map and hydrological study report was prepared as input to various regulatory approval applications.

R**ole:** Design Engineer

Responsibilities: Hydrological analysis, Hydraulic modelling, Floodline delineation and preparing the Hydrology report.

Greefspan 2 Solar Farm Hydrology, Northern Cape Province, South Africa | US$ 2 500

Client: Grupo Gransolar | **Date**: October 2019

Client Contact Details: Manuel Bolano, Project Manager; Ph +34 917 364 248

Description: SMEC was engaged by Gransolar to undertake a Hydrological and Flood Risk Assessment for the proposed Greefspan 2 Photovoltaic Solar plant in Northern Cape, South Africa. The objective of the hydrological study is to determine the external flows that will enter the site for various return periods.
Several hydrological methods, including Rational Method and SCS method were considered to calculate peak flood discharges for various return periods.
Whilst there are no defined watercourses traversing the site, local storm water will still need to be managed when the site infrastructure is developed. The input parameters generated in this hydrological study will be used to size any storm water drainage infrastructure using similar methods presented in this report.

Role: Design Engineer

Responsibilities: Hydrological analysis and preparing the Hydrology report.

Mambia PV Plant Hydrological Study, Kindia, Guinea| US$ 5 500

Client: Phanes Group | **Date**: August 2019

Client Contact Details: Guillaume Aryal, project Manager; Ph +971 55660 3166

Description: SMEC was engaged by Phanes Group to undertake a Hydrological and Flood Risk Assessment for the proposed Mambia Photovoltaic Solar Plant in Guinea, covering the following aspects:

- Hydrological Analysis
- Hydraulic Modelling
- Floodline Delineation; and
- Flood Risk Assessment.

Several hydrological methods, including Rational Method and SCS method were considered to calculate peak flood discharges for various return periods.

River hydraulics were modelled using the GeoHECRAS software suite developed by CivilGEO Engineering Software. The geometric information for the model was obtained from a drone based photogrammetric survey and roughness coefficients estimated from site surveys, based on the HEC-RAS hydraulic reference manual descriptions.

A floodline map and flood risk report was prepared as input to Environmental Authorisation process with the flood risk assessment considering the following: Depth of floodwaters; Erosion/siltation; Period of Flooding; Potential damage to infrastructure; Loss of vegetation and Loss of Life.

Role: Design Engineer

Responsibility: Hydrological analysis, Hydraulic modelling, Floodline delineation, Flood Risk Assessment and preparing the Hydrology report.

Mohale's Hoek Solar Farm, Mohale's Hoek, Lesotho | US$ 8 600

Client: Phanes Group | **Date**: July 2019

Client Contact Details: Valerio Massimo Bu, Project Manager, Ph +971 4558 7450

Description: SMEC was appointed by Phanes Group to undertake a Hydrology and Flood Risk Assessment for the proposed Mohale's Hoek Photovoltaic Solar Plant in Lesotho. The objectives of the Hydrology and Flood Risk Assessment include: Collection of historical precipitation data; Determination of design or peak floods using empirical methods, statistical/probabilistic methods and deterministic methods; Hydraulic modelling for the 10 and 100 year recurrence interval floods; Determination of 10 and 100 year floodlines using a hydraulic model; Description and determination of flood risk based on flood hazards (based on floodlines) and vulnerabilities (location of proposed critical civil, mechanical and electrical infrastructure, power stations, dwelling units, offices and solar installations); and recommendation of flood mitigation and protection measures.

Role: Design Engineer

Responsibilities: Hydrological analysis, Hydraulic modelling, Floodline delineation and preparing the Hydrology report.

Touna-Bla PV Plant, Bamako, Mali | US$ 7 500

Client: Phanes Group | **Date**: June 2019 – July 2020

Client Contact Details: Guillaume Ayral, Project Development Manager; Ph +971 55660 3166

Description: SMEC was appointed by Phanes Group to undertake a Hydrology and Flood Risk Assessment for the proposed Touna-Bla Photovoltaic Solar Plant in Mali. The objectives of the Hydrology and Flood Risk Assessment Study include: Estimation of pre-development flood magnitudes and flood hydrographs for various design recurrence intervals using at least 3 international recognised methods; Estimation of post development flood magnitudes and flood hydrographs for various design recurrence intervals using at least 3 international recognised methods; 1D Hydraulic modelling for the estimated flood peaks in order to establish the extents of the flood lines for the desired recurrence intervals, along the areas at risk of flooding.; Description and determination of flood risk based on flood hazards (based on floodlines) and vulnerabilities (location of proposed critical civil, mechanical and electrical infrastructure, power stations, dwelling units, offices and solar installations); and recommendation of flood mitigation and protection measures.

Role: Design Engineer

Responsibilities: Hydrological analysis, Hydraulic modelling, Floodline delineation and preparing the Hydrology report.

Polihali Transfer Tunnel, Polihali, Lesotho | US$ 514 000 000

Client: Lesotho Highlands Development Authority | **Date**: May 2018 – Ongoing

Client Contact Details: John Sawyer, Deputy Executive Manager; Ph +266 5225 2271

Description: Design and construction supervision of approximately 38km of water tunnels, majority TBM excavation and minority drill and blast excavation, to transfer water from the new Polihali Dam to the existing Katse Dam, all as part of Phase 2 of the Lesotho Highlands Water Project (LHWP).

Role: Design Engineer

Responsibilities: Hydrological analysis, Hydraulic modelling, Floodline delineation, Concrete Pipes Design, Drainage Channel, AutoCAD Drawings and preparing the Hydrology report.

Henrietta Photovoltaic project, Henrietta, Mauritius| US$ 6 000

Client: Bouygues Construction | **Date**: March 2018 – May 2018

Client Contact Details: Claire Sina, Project Manager; Ph +337 6399 0948

Description: The project focused on developing an Operation and Maintenance Management Plan for the proactive implementation of routine maintenance tasks and providing the municipality with a baseline for cost planning and scheduling resources. The project includes the development and implementation of the plan.

Role: Design Engineer

Responsibilities: Hydrological analysis, Hydraulic modelling Floodline delineation, and preparing the report.

AKS 100MW Photovoltaic Project, Kaduna, Nigeria | US$ 14 000

Client: Sky Power| **Date**: October 2017 – December 2017

Client Contact Details: Giorgio Mauro, Director; giorgiom@skypower.com

Description: Consultancy Services for Technical Pre-Feasibility Studies on 100MW Solar Photovoltaic PV Plant in Kaduna. The overall scope of consultancy services includes the following studies: Geotechnical study, Topographic survey, Water management study and a transport study.

Role: Design Engineer

Responsibilities: Hydrological analysis, Hydraulic modelling, Floodline delineation and preparing the water management study report.

Gamsberg Mine SWMP, Northern Cape Province, South Africa | US$ 1 175 000

Client: Black Mountain Mining | **Date**: Oct2017 – March 2018

Client Contact Details: Avinash Mamtora, Manager; Ph +27 82 881 8761

Description: Preparation of a Storm Water Management Plan for a zinc mine in the Northern Cape province of South Africa. Various measured are required to deal with storm water run-off, both clean and contaminated. These measures include drainage channels, earthen bund walls, pollution control dams, pipelines and pump stations.

Role: Design Engineer

Responsibilities: Hydrological analysis, pipeline and pump station design, Design of stormwater ponds and drainage channel designs, and preparing the design report.

Douglasdale River Improvements Phase 2, Gauteng Province, South Africa | US$ 38 900 Construction Value

Client: Douglasdale Retirement Village | **Date**: March 2017 – July 2017

Client Contact Details: Rob Fraser, Manager; Ph +27 71 863 5183

Description: After assessment of an existing dam situated within the Douglasdale Retirement Village, it was concluded that its spillway capacity was inadequate with a high risk of overtopping the earth-fill embankment. A design was prepared for the upgrade of the spillway to increase its discharge capacity. The watercourse upstream of the dam is prone to erosion. To prevent further erosion of the riverbanks, several erosion control measures were investigated. An erosion control weir was proposed as the most suitable rehabilitation and prevention measure.

Role: Design Engineer

Responsibility: River hydraulics modelling and detailed design of erosion control weirs, and preparing the report.

Loopspruit Floodlines, Gauteng Province, South Africa | US$ 7 000

Client: Shangoni Management Services (Pty) Ltd

Client Contact Details: Nico Brits Manager; Ph +27 12 807 7036

Description: Determination of 1:50 and 1:100-year floodlines for a 2.5 km reach along the Loopspruit River as part of a Water Use Licence Application for a mine.

Role: Design Engineer

Responsibility: Hydrological analysis, river hydraulics modelling and preparing the report.

Verref Pollution Control Dam, Gauteng Province, South Africa | US$ 6 000

Client: Shangoni Management Services | **Date**: May 2017 – November 2017

Client Contact Details: Dawie Marre, Manager; Ph +27 12 807 7036

Description: Assessment of an existing Pollution Control Dam (PCD) to check compliance with the sizing requirements of Regulation No. 704 of the National Water Act, 1998 (Act No. 36 of 1998) which regulates the use of water for mining and related activities aimed at the protection of water resources.

Role: Design Engineer

Responsibility: Hydrological analysis of the dam using a water balance model and the concept design of a new pollution control dam; and preparing the report.

Vorna Valley River Hydraulics Management, Gauteng Province, South Africa | US$ 1 400 000

Client: Johannesburg Roads Agency (JRA) | **Date**: Sep 2016 – April 2018

Client Contact Details: Andre Nel, Planning Manager; Ph +27 82 492 2363

Description: The Vorna Valley watercourse in Midrand regularly floods adjacent properties and has eroded severely in some areas. The project aims to investigate these problems and to implement measures to address them.

Role: Design Engineer

Responsibility: Hydrological analysis, surveying, determining the flood lines and the feasibility of various proposed solutions using GeoHECRAS, designing the flood protection berms, designing gabions for erosion control as well as flood protection, and designing various riprap-lined channels, stilling basins and groynes.

Douglasdale River Improvements Phase 1, Gauteng Province, South Africa | US$ 42 800 Construction Value

Client: Douglasdale Retirement Village | **Date**: Feb 2016 – Nov 2016

Client Contact Details: Rob Fraser, Manager; Ph +27 71 863 5183

Description: Civil Engineering designs on the Stormwater stream running through Douglasdale Retirement Village were required. These designs included: Gabion designs and Rockfill sand trap design (weir).

Role: Design Engineer

Responsibility: Producing the hydrology flood estimation, gabion designs for bank erosion protection and the weir design, site surveying, site monitoring and BOQ.

Tharisa Rail Project, North West Province, South Africa | US$ 35 000 00

Client: Transnet and Tharisa Minerals | **Date**: Feb 2016 – March 2016

Client Contact Details: Lazarus Rapetswa, Manager; Ph +27 12 315 2525

Description: Transnet freight rail and Tharisa Minerals entered a Public Private Partnership to construct a new link line into Tharisa mine, near Marikana, providing access to a new load-out station that will be capable of loading a 150-wagon train.

Role: Hydrologist

Responsibility: Hydrological analysis.

Devland Community Education Campus, Gauteng Province, South Africa | US$ 376 000

Client: Growing up Africa | **Date**: Nov 2017 – Dec 2017

Client Contact Details: Deborah Terhune, CEO; Ph +27 82 826 2237

Description: Growing Up Africa (GUA), A non-profit organization based in the USA is building a multi-purpose community centre in the Devland community located in Soweto. The centre is a single storey educational facility.

Role: Construction Monitor

Responsibility: Responsible for site monitoring as well as land surveying on site.

Courses & Conferences attended

2016:	SAICE Ingula Pumped Storage Scheme (1 day site visit)
2017:	The CAD Corporation AutoCAD Essentials course (4 days)
2017:	CESA Technical and Business report writing (3 days)
2017:	The CAD Corporation Civil 3D Essentials course (4 days)
2017:	CoJ Stormwater By Laws training workshop (2 days)
2017:	CESA YPF BBBEE debate (1 day)
2018:	SAICE 2017 Infrastructure Report Card Breakfast workshop (1 day)
2018:	SARF Drainage Manual course (2 days)

Johan Badenhorst

Technical Specialist

Personal Information

- ID no.: 560814 5127 085
- Nationality: South African

Years of Industry Experience

- 43 years

Qualifications and Memberships

- National Diploma for Technicians-Engineering Survey, Cape Technicon, 1980
- National Diploma for Technicians-Civil Engineering, Cape Technicon, 1991
- B.Tech Civil Engineering, Technicon Free State, 2002
- Professional Technologist with Engineering Council of South Africa, No. 201170260

Key Skills and Competencies

- Tunnel horizontal and vertical alignment design by DTM and CAD modelling
- Road and Railway Geometric design
- Canal geometric and hydraulic design
- Topographic Survey
- Site Supervision of Tunnel works, concrete structures
- Setting up monitoring and reporting systems for TBM and D&B tunnels

Professional Overview

Johan Badenhorst is a Professional Technologist and a Survey Technician with 24 years of experience in engineering, topographical survey work and construction site supervision, as well as 18 years' experience in the design environment.

His experience includes:

- Construction monitoring of tunnel works, concrete structures, road earthworks and layerworks, and water, sewerage and stormwater reticulation systems.
- Setting up monitoring and reporting mechanisms for TBM and D&B tunnel excavation alignments.
- Tunnel horizontal and vertical alignment design using DTM and CAD modelling.
- Road and Railway Geometric design.
- Canal geometric and hydraulic design.
- Topographic survey and setting out, using total stations, and levelling equipment, for design and construction of bridges, roadworks, earthworks and underground excavations (including both drill and blast and TBM tunnelling) and buildings.
- Processing of topographical, ground survey and aerial survey data into Digital Terrain Models.
- Procurement of survey services, including ground control surveys and aerial mapping (LiDAR).
- Hydrological and River hydraulics modelling.

Relevant Project Experience

Trojena | R500 million plus (Project Value)

Client: NDA | **Date:** October 2023 - Date

Client Contact Details: NDA

Description: Infrastructure development in mountainous terrain in Saudi Arabia.

Role and Responsibilities: Technical and CAD support. Concept design of excavations and earthworks for water treatment and water tank platforms on steep and undulating slopes.

Stompdrift Kammanassie Water Security Study -Inception | R 377 800 (fees)

Client: Stompdrift - Kammanassie Water Users Association| **Date**: August 2022 - Date

Client Contact Details: Willem Fourie, SKWGV, PO Box 164 Oudtshoorn – (+27 44 272 2751)

Description: The SKWGV required the review of previous studies and recommendations on strategies and methos to improve the water security within the Irrigation Scheme.

Role and Responsibilities: Technical support. Review of previous studies, evaluating of the information, conclusions and recommendations presented within these studies. Preparation of a short list of the recommendations as presented including the presentation of additional strategies. The final list of recommended strategies includes raising of the Kammanassie Dam, inspection of the existing canal and upgrading of canal lining and the provision of intermediate storage dams along the distribution canal.

Katse Delivery Tunnel No. 2 Plugging, Lesotho | R12 960 000 (fees)

Client: LHDA – Operations Branch | **Date:** August 2022 to Date

Client Contact Details: Chakala E Mphafi, Engineer Civil - Contracts Admin, (+266) 22246000 or (+266) 22311280, mphafic@lhda.org.ls

Description: The Katse Dam Diversion Tunnel No.2 outlet works require to be permanently plugged. The works comprise sealing off the steel lined tunnel with a steel bulkhead, back filling the chamber between the gates with concrete/grout, back filling the gate operating gallery with concrete and ancillary works.

Role and Responsibilities: Technical and CAD support. Coordination of the production of the tender documents and specifications, layout drawings, estimation of quantities and cost to tender design levels, input into the Design Report. Tender evaluation and compilation of the Tender Evaluation Report with recommendations to the Client.

Pandora Dam (fees) | R2 415 000 (fees)

Client: Sibanye Gold Shared Services (Proprietary) Limited| **Date**: March 2022 – October 2022

Client Contact Details: Cobus Pieters, Superintendent Engineering SR, +27 (0)14 571 5428, Cobus.Pieters@sibanyestillwater.com

Description: Sibanye Stillwater requires a buffer storage for raw water from the Hartbeespoort Canal. An off-stream storage dam with a capacity of 30 000 m^3 was designed.

Role and Responsibilities: Dam and road design using Civil 3D, estimation of quantities and cost to detail design levels, input into the Design Report.

Ferreira Canal, ESwatini | USD 27 000 (fees)

Client: eSwatini Electricity Company | **Date**: January 2022 – March 2022

Client Contact Details: Charles Coleman, Power Stations Manager, +268 550 2611, charles.coleman@sec.co.sz

Description: The Edwaleni Hydropower Station receives water from the Little Usutu and the Great Usutu rivers via two canals; the Main Canal and the Ferreira Canal respectively. This project entails the design of improvements to the Ferreira Canal (approximately 7.2 km in length and predominantly unlined) to increase the flow capacity to 6m^3/s, by enlarging and lining.

Role and Responsibilities: Technical and CAD support. Production of a Civil 3D model, estimation of quantities and cost to preliminary design levels, input with regards to constructability to the Preliminary Design Report.

NEOM Industrial City Phase 3, Kingdom of Saudi Arabia | USD 1 734 400 (fees)

Client: Surbana Consultants PTE.LTD | **Date**: August 2021 – February 2022

Client Contact Details: Ruban Muruganandan, M +971 50 2089856 (UAE), Ruban.muruganandan@surbanajurong.com

Description: Phase 3 Design Consultancy Services for NEOM Industrial City Site Wide Infrastructure.

Role and Responsibilities: Technical support and CAD management for potable water reticulation layouts. Support to procurement process of topographic survey and satellite imagery and elevation models of the project area.

Wabag Hydro Power Project, Papua New Guinea | USD 27 000 (fees)

Client: SMEC Asia | **Date**: July 2021 – June 2021

Client Contact Details: Simon Tundua, simon.tundua@smec.com

Description: Hydro Power Project., review of design report.

Role and Responsibilities: Technical Support. Review and report on specific aspects of the detail design report, feasibility study report and design drawings for the Wabag Hydropower station development project.

The aspects reviewed include layout drawings, tunnel construction drawings, and proposed construction methodologies

Julius Nyerere Hydro Power Project, Tanzania | USD 13 710 (fees)

Client: SMEC Africa | **Date**: June 2021 – September 2021

Client Contact Details: G Marra, Program Manager, giuseppe.marra@smec.com

Description: Hydro Power Project., verification of Saddle Dam material quantities.

Role and Responsibilities: Technical Support. Compute the quantities of the materials in the earthworks of Saddle Dams 2, 3 and 4. The computation entailed creating complex assemblies in AutoDesk Civil 3D and deriving volumes for the material in 8 separate zones of the earthworks.

Sha Tin Caverns, Hongkong | USD 27 883 (fees)

Client: SMEC Asia | **Date**: June 2021 – July 2021

Client Contact Details: Alexi Bhanja, Managing Director, '+852 3995 8100, alexi.bhanja@smec.com

Description: Construction of underground caverns to relocate the Sha Tin WWTW from above-ground to below-ground to free up space for development. SMEC undertook the tender design of the caverns for a tendering contractor, with particular emphasis on the design of temporary support.

Role and Responsibilities: Technical and CAD Support. Review of Contractor's construction methodologies.

Calitzdorp Dam, Western Cape, South Africa| R 130 000 (fees)

Client: Calitzdorp Export Agri Hub | **Date**: October 2021 – November 2021

Client Contact Details: Gerhard Meyer, +27 82 802 7138

Description: Water Resource Study to investigate the feasibility of the proposed Calitzdorp Spa Dam.

Role and Responsibilities: Technical Support. Digital Terrain modelling four possible dam sites and developing dam capacity curves. Developing high level costing to compare the respective sites.

Nzove 1 WTW, Kigali, Rwanda | R 2.5 million (fees)

Client: WASAC, Rwanda | **Date**: November 2020 – December 2020

Client Contact Details: Joseph Ndagijimana, Project Manager, WASAC, Kigali, Rwanda | jndagijimana@wasac.rw

Description: Refurbishment of 15 ML/day Water Treatment Works and Transmission Main.

Role and Responsibilities: CAD and Technical Support. CAD drafting support, including conversion of scanned plans to AutoCAD drawings. Technical support included gathering on site data of pumps, piping, pressure vessels, and other components.

Begota Dam, KwaZulu-Natal Province, South Africa | US$ 47 000 Fees

Client: IFA | **Date:** June 2020 – August 2020

Client Contact Details: Howick Oosthuizen; Development Manager; +27 83 463 5279

Description: Design of Begota Dam, a clay core earth dam of approximately 10m height and storage capacity of 7,000m³, complete with concrete side-channel spillway and stilling basin, with culverts to enable a road crossing.

Role and Responsibilities: Technical Specialist. Review and revision of Dam embankment drawings.

Lobatse Water Supply Master Plan Design-Build Bid, Botswana | US$ 100 000 Fees

Client: PowerChina | **Date**: June 2020 – July 2020

Client Contact Details: George Zhao; Engineer; +27 (0)717165460 / +26 (0)964539986.

Description: The Water Utilities Company of Botswana let a tender for the Design and Construction of the Lobatse Water Supply Master Plan. The project includes: a 60 km long 900 mm diameter steel pipeline from Gaborone to Lobatse, a new 6 MW pump station in Gaborone, 3 new reservoirs, two 600 mm ductile iron ring main pipelines and associated infrastructure. As the client had not provided substantial designs or bills of quantities, a prospective Contractor required engineering services to prepare tender designs and bills of quantity to enable pricing of his bid.

Role and Responsibilities: Technical Specialist. Responsible for measuring quantities and preparation of bills of quantities for several reservoirs as input to Contractor's Design-Build bid for the construction of the project.

LHWP Delivery Tunnel North Outage, Free State | US$ 1.1 million Construction Value and Fees

Client: Trans Caledon Transfer Authority| **Date**: October 2019 – November 2019

Client Contact Details: David Keyser; Head of Engineering; Ph +27 12 683 1200

Description: Inspection of the tunnel lining and identification of areas requiring repair.

Role and Responsibilities: Inspector and Construction Supervisor. Supervising of the contractor's repair procedures, advising of areas to be repaired and repair methods. Research into and evaluation of repair products.

Polihali Transfer Tunnel, Lesotho | US$ 8.86 million Fees

Client: Lesotho Highlands Development Authority **Date**: January 2018 – January 2022

Client Contact Details: John Sawyer, Deputy Executive Manager; Ph +266 5225 2271

Description: Design and construction supervision of approximately 38km of water tunnels, majority TBM excavation and minority drill and blast excavation, to transfer water from the new Polihali Dam to the existing Katse Dam, all as part of Phase 2 of the Lesotho Highlands Water Project (LHWP).

Role and Responsibilities: Designer and Cost Engineer. Geometric alignments of tunnel and access adits, earthworks modelling, access road design, cost estimates, preparation of specifications and tender documents.

Investigate on emergency medical response and air evacuation for MSKC employees and reported back to the Project Manager. Planned and conducted the voluntary site visit to show the project areas to approximately 60 attendees over a 2-day site visit. Managed the editing of drone videos taken of the project area and added a voice over to the final videos used in the tender presentation.

Tina Falls EIA, Eastern Cape | US$ 35 500 Fees

Client: Sidala Energy Solutions | **Date**: August 2017 – September 2017

Client Contact Details: Christiaan Bode; Project Manager; Ph (+27) 082 822 4792]

Description: Preparation of a site layout plans for an environmental impact assessment for a mini hydro power plant in the Eastern Cape province of South Africa. Layouts of construction areas, access roads and electrical power line connections.

Role and Responsibilities: Designer. Site Layout Evaluation, digital terrain modelling and drawing preparation.

Gamsberg SWMP, Northern Cape | US$ 1.17 million Construction Value

Client: Black Mountain Mining | **Date**: August 2017 – November 2017

Client Contact Details: Mamtora Avinash, Manager; Ph +27 82 881 8761

Description: Preparation of a storm water management plan for a zinc mine in the Northern Cape province of South Africa. Various measures are required to deal with storm water run-off, both clean and contaminated. These measures include drainage channels, earthen bund walls, pollution control dams, pipelines and pump stations.

Role and Responsibilities: Designer. Geometric and Digital Terrain modelling.

Polihali Diversion Tunnels, Lesotho | US$ 39.0 million Construction Value

Client: Lesotho Highlands Development Authority | **Date**: November 2016 – December 2017

Client Contact Details: John Sawyer, Deputy Executive Manager; Ph +266 5225 2271

Description: Design and construction supervision of twin diversion tunnels to enable the construction of the proposed 163 m high Polihali Dam. The Polihali Dam will form part of Phase 2 of the Lesotho Highlands Water Project (LHWP).

Role and Responsibilities: Designer and Cost Engineer. Geometric alignments, earthworks modelling, access road design, cost estimates, preparation of specifications and tender documents.

Thwake Multi-Purpose Dam, Kenya | US$ 105.2 million Construction Value

Client: Kenyan Ministry of Water and Irrigation | **Dates**: June 2016 - August 2021

Client Contact Details: Mr Musembi Munyao, Manager; Ph +27 12 315 2525

Description: The project entails design of a new CFRD dam. Construction of the dam requires a river diversion, by means of 2 x 12m diameter, 750m long diversion tunnels through the right abutment, which are to be converted into a low level outlet and hydropower penstock conduit routed from an intake tower in the latter stages of construction of the dam.

Role and Responsibilities: Design Technologist. Layouts of the approach channels and platform, measurement of tender earthworks quantities, provision of computer aided design and drafting and assistance in selection of tunnel monitoring system and instrumentation.

Tharisa Rail Siding, Marikana, North West Province| R 34.92 million Construction Value

Client: Transnet Capital Projects | **Dates**: March 2016 - June 2017

Client Contact Details: Lazarus Mapetswe, Manager, +24 (0) 11 583 0372

Description: Design of a 10.5km long rail line branching off to Tharisa Mine from the main Pyramid-Marikana line. The design incorporated vertical and horizontal alignment, two road-over-rail bridges, two rail-over-road bridges, eleven drainage culverts, level crossings, road re-alignment and OHTE.

Role and Responsibilities: Design Technologist. Geometric design of the rail horizontal and vertical alignments, and turnout from the mainline. Drainage design including the design of the storm water culvert and the hydrology. Coordinating interface between the various contributing engineering disciplines. Quantity measurement for the bill of quantities.

Maremani Nature Reserve, Sedimentation Control and Mitigation Plan, Limpopo Province, South Africa | US$ 19 500 Fees

Client: Maremani Trust | **Date**: June 2015 – September 2015

Client Contact Details: Reiker Botha, Manager; Ph (+27) 84 652 9879

Description: The project entailed identifying and designing solutions to the ongoing sedimentation of the Maremani Dam in the Nzhelele River.

Role and Responsibilities: Project Lead and Design Technologist. Identifying the sources and estimating the quantities of sedimentation, design of remedial and mitigation measures and reporting on the proposed remedial and mitigation processes.

University of Pretoria, Improvements to River works | US$ 29 000 Construction Value

Client: University of Pretoria Facilities Management| **Date**: May 2015 – June 2016

Client Contact Details: Prof Schalk Claasen, Project Manager; Ph +27 12 420 2433

Description: Tender design, procurement and construction monitoring of improvements to the Hartbeesspruit stream through the LC De Villiers Sports Grounds, encompassing spillway and embankment repair to a failed dam, erosion control weirs and gabions and regeneration of an existing wetland.

Role and Responsibilities: Design Technologist and Technical Project manager. Design of the weir structures. Compiling of contract document including the Bill of Quantities. Site supervision of the various concrete works.

Kafue Gorge Lower Hydroelectric Project, Zambia | US$ 1.97 Billion Construction Value

Client: ZESCO (formerly Zambia Electricity Supply Corporation Limited) | **Date**: April 2015 – July 2015

Description: Provision of an Engineer's Estimate of the cost for the design and construction of the proposed Kafue Gorge Lower Hydro Electric Project.

Role and Responsibilities: Costing Engineer. Reviewing construction unit rates and adjusting such rates from the base date to the current date. Carried out checks on measured quantities. Liaising with a professional quantity surveyor to provide construction rates specific to Zambia and the relevant time frame.

Gautrain Rosebank Station Carpark Extension, Gauteng Province, South Africa | US$ 230 000 Fees

Client: Bombela Concession Company | **Dates:** November 2014 – June 2015

Client Contact Details: Tawanda Shamu, Project Manager; Ph +27 11 446 6804

Description: Design of the vertical extension of the Rosebank Gautrain car park from two levels to four levels. Involved a geotechnical review and design of the foundation loading, structural design of additional levels, extension of lift shaft and ancillary mechanical and electrical systems, and drainage and parking layout designs. A traffic impact study was also completed on the adjacent road network and entrance and exit of the parking area.

Role and Responsibilities: Technical Specialist. Responsible for co-ordination of production of the technical deliverables by the architectural, structural, mechanical, electrical, fire and traffic disciplines and obtaining the required approvals.

ABL Brewery Development – Accra, Ghana

Client: SAB Miller | **Date:** July 2014 – September 2014

Description: Expansion and upgrading the SAB Miller Accra brewery and ancillary structures, including erection of large water tanks, mass tanks, concrete bases, stormwater, sewage and industrial effluent reticulation.

Role and Responsibilities: Resident Engineer SAB Miller. Construction Supervision. Review of design drawings, bills of quantities, measurement specification and Health and Safety guidelines.

University of Pretoria Addendum to Stormwater Management Plan (Pretoria/Gauteng Province, South Africa)

Client: University of Pretoria Facilities Management | **Date**: February 2014 – March 2014

Client Contact Details: Prof Schalk Claasen, Project Manager; Ph +27 12 420 2433

Description: Addendum to Stormwater Management Plan to include the effect of the proposed Ox Street access.

Role and Responsibilities: Technical Specialist. Analysis of the effect of the proposed Ox Street access road on the Hartebeest Spruit river hydraulics, using River Analysis and HEC-RAS software and reporting on the results.

PRASA Rolling Stock Renewal Project (South Africa)

Client: Passenger Rail Agency of South Africa | **Date**: April 2013 – July 2014

Description: Provision of technical assistance to PRASA in the Upgrading of the Rolling Stock Maintenance Depots in major centres, including conceptual designs and the procurement of topographical and services surveys, terrestrial building scanning to produce structural and civil engineering drawings of the existing building and geotechnical investigations.

Role and Responsibilities: Technical Specialist. Managing the procurement of and supervising the commissioning and execution of the site investigations (topographical surveys, geotechnical investigations, terrestrial building scanning and services detection). Managing and distributing the data receipts and deliveries, and the contractor is invoicing. Review of the Braamfontein Depot Upgrade civil infrastructure design drawings.

Nairobi Water Supply Tunnel (Nairobi, Kenya)

Client: Athi Water Services Board | **Date**: May 2013 – September 2013

Description: Water transfer tunnel.

Role and Responsibilities: Technical Specialist. Review of design drawings, bills of quantities, measurement specification and Health and Safety guidelines.

Limpopo Farm Dams (Limpopo Province, South Africa)

Client: Limpopo Provincial Government Department of Agriculture | **Date:** February 2013 – April 2013

Description: Repair of thirteen farm dams damaged during floods.

Role and Responsibilities: Technical Specialist. Assisting with drafting services and the design of the repairs for one of the dams.

Incomati River Diversion Weir (Xinavane, Mozambique)

Client: Tongaat Hulett | **Date:** January 2013 – July 2013

Client Contact Details: Evaristo Mubaya; Agricultural Services Manager; Ph +258 85 874 6396

Description: Concept weir design for water supply to Xinavane Sugar Mill.

Role and Responsibilities: Project manager. Liaising with the Client to determine scope of works. Managing the execution of the concept design.

Indonesia Hydropower Study (Bengkulu, Indonesia)

Client: PT Green Investments | **Date:** January 2013 – February 2013

Description: Hydropower viability study.

Role and Responsibilities: Technical Specialist. Compiling catchment areas from supplied mapping and satellite Radar Terrain Modelling data.

Lesotho Highlands Water Project (Lesotho)

Client: Trans Caledon Tunnel Authority | **Date:** June 2012 – November 2012

Description: Tunnel maintenance and operation including refurbishing of control and dewatering valves, refurbishing of steel lining coatings and the replacement and installation of existing and new instrumentation.

Role and Responsibilities: Technical Specialist. Managed and supervised the procurement, installation and commissioning of instrumentation to monitor water levels at strategic points within the Transfer and Delivery Tunnels to assess the tunnel flow characteristics. Tasks included the concept design of the mountings for the Radar Level Sensors installations on the Katse Inlet Tower, Muela Surge Shaft and Muela Dam wall.

Witbank Rail Yard Storm Water Condition Assessment (Witbank/Mpumalanga Province, South Africa)

Client: Transnet Capital Projects | **Date:** August 2012 – November 2012

Client Contact Details: [Roger Traill; Project Manager; Ph (+27) 083 455 6305]

Description: Investigation of the storm water management capabilities and deficiencies of the Witbank Transnet Rail Yard.

Role and Responsibilities: Technical Specialist. The investigation and compiling the report detailing the problems identified with regard to deficiencies, damage, health and safety issues. The report also outlined proposed future action to remedy the problems identified, together with concept budgets.

University of Pretoria Projects (Pretoria/Gauteng Province, South Africa)

Client: University of Pretoria Facilities Management | **Date:** June 2012 - July 2013

Client Contact Details: David Viljoen; Project Manager; Ph (+27) 083 640 3447

Description: Groundwater ingress control at Law Faculty.

Role and Responsibilities: Technical Specialist. The design and project management groundwater control measures consisting of subsoil drainage and a sump pump station at the UP Law Faculty building to prevent groundwater rising in the classrooms during the rain seasons.

Kruisvallei Hydropower Projects (Bethlehem/Freestate Province, South Africa)

Client: Kruisvallei Hydro | **Date:** July 2012 – March 2013

Client Contact Details: Christiaan Bode; Project Manager; Ph (+27) 082 822 4792

Description: Two proposed hydropower projects on the Ash River at pre-feasibility and advanced concept levels.

Role and Responsibilities: Design Technologist. Geometric layouts of the canals associated with the hydropower infrastructure. Tasks included canal cross section designs, research into turbines, trash racks and isolation gates, and the preparation of bills of quantities

University of Pretoria Projects (Pretoria/Gauteng Province, South Africa)

Client: University of Pretoria Facilities Management | **Date:** March 2011 – June 2012

Client Contact Details: David Viljoen; Project Manager; Ph (+27) 083 640 3447

Description: Storm water damage prevention measures.

Role and Responsibilities: Design Technologist and Project Manager. Design, project management and site supervision of the storm water diversion measures to prevent flooding of the High Performance Centre building during large storms.

Mokolo Crocodile West Augmentation Project (Limpopo, South Africa)

Client: Trans Caledon Tunnel Authority | **Date:** April 2008 – February 2011

Client Contact Details: Mr David Keyser, Project Manager; Ph +27 12 683 1203

Description: Water transfer scheme to provide inter alia water from the Mokolo Dam to the Medupi Power Station development near Lephalale.

Role and Responsibilities: Mapping Technologist. Managing the procurement of the Aerial Mapping by LiDAR survey, (including the control survey and cadastral mapping). Assisting with the gathering and distribution of existing mapping and aerial survey information. Managed the independent terrestrial quality check on the aerial survey and mapping

A-Prep Locomotive Depots for Transnet (Johannesburg/Gauteng Province, South Africa)

Client: Transnet Capital Projects | **Date:** May 2010 – January 2011

Client Contact Details: [Roger Traill; Project Manager; Ph (+27) 083 455 6305]

Description: Design and construction of new workshops to service and maintain locomotives.

Role and Responsibilities: Design Technologist. Provided assistance with the preparation of the tender and design drawings. Additional responsibilities included calculation of horizontal and vertical geometric alignments for the rail connection between the exiting yard and the workshop, and design of stormwater pipes and outlet structure.

Moatize – Nacala Rail Tunnel (Malawi, Mozambique)

Client: Aurecon | **Date:** June 2010 – August 2010

Client Contact Details: [Dr Eduard Vorster; Project Manager; Ph (+27) 12 427 2000]

Description: Proposal for tunnel alternatives on rail route.

Role and Responsibilities: Design Technologist. Compiled Digital Terrain Models to investigate proposed tunnels on rail alignment, including calculation of horizontal and vertical tunnel alignments.

SARCC 2010 Interventions (Johannesburg/Gauteng Province, South Africa)

Client: Passenger Rail Agency of South Africa | **Date:** May 2008 - June 2010

Client Contact Details: [Tonie Vermeulen; Project Manager; Ph +27 83 275 1524]

Description: Provision of a 2 km connecting link rail between the Kaserne and Langlaagte rail line to avoid shunting through the New Canada Station.

Role and Responsibilities: Design Technologist. Preparation of the conceptual and construction design drawings, including horizontal and vertical geometric alignments of the slip link and staging yard rail lines to the PRASA geometric standards. The geometric design included the positioning of crossovers and a rail over road bridge alignment. Assisted with the procurement of the topographical surveys.

Florida Lake to Fleurhof Dam Canal (Johannesburg/Gauteng Province, South Africa)

Client: Council for Geoscience | **Date:** May 2006 - July 2010

Client Contact Details: [Mr J Hugo; Financial Manager; Ph +27 (0)12 841 1911]

Description: Canalization (with a waterproof membrane) of a water course above shallow undermining to prevent ground water entering the mine workings and therefore contributing to the acid mine drainage problems in the Central Wits Basin

Role and Responsibilities: Design Technologist, Project Manager and Site Supervisor. Design of the canal geometry. The geometric design was done to balance cut and fill. Project management and site supervision was carried out in the initial stages of the project.

Lesotho Highlands Water Project Further Phases Study (Lesotho)

Client: Trans Caledon Tunnel Authority | **Date:** January 2006 - December 2009

Client Contact Details: Leon Tromp; Study Coordinator; +266 5221 4035

Description: Feasibility study into the Lesotho Highlands Water Project further phases.

Role and Responsibilities: Design Technologist. Preparation of conceptual design drawings and management of CAD drafting team. Preparation of the Tunnel horizontal and vertical alignment options. Evaluation and comparative costing of possible pipeline options to convey water from below the Katse Dam to Katse Dam. Assisted with the procurement of the control survey by a firm of Lesotho based surveyors. Managed the procurement of the Aerial Mapping by LiDAR survey, (prepared the tender documents, evaluated the tenders, and drafted recommendation to client, certified payments to the contractor). Assisted with the management and distribution of mapping information procured for the study and existing information from previous studies.

Gautrain Rapid Rail Link – Viaduct Drainage (Johannesburg/Gauteng Province, South Africa)

Client: Bombela Construction Joint Venture | **Date:** August 2006 – January 2009

Client Contact Details: [Peter Squires; Project Manager; Ph 031 240 7300]

Description: Design of the seven viaducts on the southern portion of the Gautrain Rapid Rail

Role and Responsibilities: Design Technologist. Design and preparation of the pipe layouts for the deck drainage of the Viaducts on the southern portion of the Rapid Rail Link Project, including pipe sizing for capacity, pipe schedules and typical installation details.

ERPM Mine Decanting Tunnel (Johannesburg/Gauteng Province, South Africa)

Client: Council for Geoscience | **Date:** November 2005 - February 2006

Client Contact Details: [Mr J Hugo; Financial Manager; Ph +27 (0)12 841 1911]

Description: Proposed decanting tunnel to lower water levels in the ERPM mine.

Role and Responsibilities: Design Technologist. Designing the tunnel horizontal and vertical alignments, conceptual design drawings and estimates. Further did preparatory work and drawings for the geotechnical investigation for the proposed tunnel.

Mamelodi Outfall Sewer Tunnel (Tshwane/Gauteng Province, South Africa)

Client: Thwane Municipality | **Date:** February 2004 – September 2008

Client Contact Details: Mr J Wessels

Description: Outfall Sewer Tunnel

Role and Responsibilities: Design Technologist, Resident Engineer. Tunnel horizontal and vertical alignment design including basic hydraulic analysis to determine the tunnel profile. Portal layouts. Prepared tender and construction drawings. Estimated quantities for geotechnical investigation. Resident engineer for latter part of contract performing site supervision of drill and blast activities, concrete lining, cavity grouting and invert lining, including preparation of monthly payment certificates and progress reports.

Guatrain Rapid Rail Link Tender Design (Gauteng Province, South Africa)

Client: Gauliwe JV | **Date:** October 2002 - August 2004

Client Contact Details: Mr K van der Hoven

Description: Rapid Rail

Role and Responsibilities: Design Technologist. Assisted with design of the station layouts in the tunnelled sections of the rail alignment, the sectional envelopes and equipping of the single and double track drill and blast tunnels and the TBM tunnels, preparation, drafting and checking of tender design drawings. Obtained and calculated design parameters for input into the determination of the horizontal and vertical alignments in the tunnelled sections. Responsibilities further included determination and measurement of quantities and draughting of the schedules of quantities and assistance with the preparation of the geotechnical drawings. Also prepared and compiled a monitoring procedure to determine and quantify any possible ground settlement along the tunnel routes.

Mohale Tunnel (Intake), Lesotho Highlands Water Project (LHWP) Phase 1B. (Lesotho)

Client: LHDA | **Date:** May 1998 - February 2004

Client Contact Details: Mr C Makwalumba

Description: Water Transfer Tunnel

Role and Responsibilities: Chief Surveyor. Co-ordinated and managed the survey team to check the contractors setting out and as built positions of works. Responsibilities included the survey of original ground for design, measurement of fencing, survey and reporting on the as-built construction of the TBM tunnel and D&B adits. Also sourced and procured survey and computer equipment and supervised construction of earthworks. Acted as office engineer responsible for the management and maintenance of the computer network.

Completed surveys for final Quantities and As-built Drawings. Also set out and supervised the construction of the tunnel maintenance gate shaft access road (600m long). Completed the survey and reported on site investigation for relocation of police accommodation at Setibeng Police Post.

Matsoku River Division, Lesotho Highlands Water Project (LHWP) Phase 1B. (Lesotho)

Client: LHDA | **Date:** February 1998 – April 1998

Client Contact Details: Mr C Makwalumba

Description: Water Transfer Tunnel

Role and Responsibilities: Chief Surveyor. Sourced and procured survey instruments required for the contract. Survey of original ground for design purposes, survey of cultivated fields for compensation purposes. Survey and map the installation of rock-bolts installed for the stabilisation a rock cutting. Compiled asset lists of the serviceable furniture in the staff housing and the required replacement furniture, placing furniture in staff housing as assigned.

Ebony Park Extension 4. (Gauteng)

Client: City of Johannesburg | **Date:** November 1997 – January 1998

Description: Township Development

Role and Responsibilities: Resident Engineer. Construction supervision of a township development, installation of water and sewer reticulation and roads, sourcing of materials for rehabilitation.

Johannesburg International Airport. (Gauteng)

Client: Engen | **Date:** May 1997 – October 1997

Description: Elevated filling station and parking garage

Role and Responsibilities: Resident Engineer. Construction supervision of the deck for an elevated filling station (the first in South Africa), an adjacent 6 level parking garage, approach ramps, earthworks, bored pile foundations, subsurface drainage and traffic accommodation.

Katse Dam, LHWP Phase 1A. (Lesotho)

Client: LHDA | **Date:** June 1996 – April 1997

Client Contact Details: Mr C Makwalumba

Description: Large Concrete Arch Dam

Role and Responsibilities: Senior Surveyor. Calculate setting out details for the ogee spillway concrete works and check the actual setting up of the shuttering to an accuracy of better than 5mm. Check and control the final adjustments for the screed rails that determined the crown levels. Check setting out and positions of the pre-cast elements in the spillway and box beam bridge over the spillway. Liaise with the Contractor's Survey Department to provide details and records of setting out to the Engineer. Survey as-built positions of concrete works.

Delivery Tunnel South, LHWP Phase 1A. (Lesotho)

Client: LHDA | **Date:** June 1991 – August 1991; January 1996 – May 1996

Client Contact Details: Mr C Makwalumba

Description: Water Transfer Tunnel

Role and Responsibilities: Senior Surveyor. Collate the computer records of this contract's construction drawings and contractual correspondence from backup discs and transfer this material onto computer tapes for archiving on Compact Discs (CDs). Complete as-built surveys and check surveys.

Delivery Tunnel North, LHWP Phase 1A. (Free State, South Africa)

Client: LHDA | **Date:** September 1991 – January 1996

Client Contact Details: Mr C Makwalumba

Description: Water Transfer Tunnel

Role and Responsibilities: Chief Surveyor. Check-survey of the Contractor's survey network for controlling the TBM tunnelling direction by separate independent horizontal and level traverses, corrected using the gyro bearings surveyed by an independent sub-contractor. Check the as built tunnel alignment, compare with design and report the results as numerical values. Survey and prepare contour plans and sections for design. Check survey construction of earthworks and concrete works at the portals. Survey spoil-dump positions, shapes and volumes. Check survey installation of the 4 m diameter steel liners in the river crossing and low cover areas.

Marlboro Interchange, Sandton. (Gauteng, South Africa)

Client: City of Johannesburg | **Date:** January 1990 – June 1990

Description: Infrastructure Development

Role and Responsibilities: Senior Surveyor. Plan and design road deviation and road signage according to TPA specifications and supervise the implementing of the road deviation. Check survey layer-works and horizontal alignment of the road works. Detailed level survey of the paved surface of the triple intersection. Check installation of a water pipeline (60 mm and 300 mm diameter steel pipes & valve works) and calculate the bend angles and positions for a road crossing. Supervise the positioning and painting of road-markings.

Houwteq Access Road and Infrastructure, Grabouw. (Western Cape, South Africa)

Client: Houwteq | **Date:** September 1988 – December 1989

Description: Infrastructure Development

Role and Responsibilities: Senior Surveyor. Check survey layer-works and horizontal alignment of the road works. Survey setting out of a concrete road and truck arrestor bed built at a steep (16%) slope. Calculate and set out intersections of steep roads and stormwater control structures. Survey long and cross sections for calculating and setting out the alignment for a large Armco pipe culvert underneath a spoil-dump. Survey and calculate end positions of pipe culverts under the ring road. Check the setting out and as-built positions of a water-supply works, consisting of a 5km pipeline, three pump-stations, concrete reservoir, etc. Supervise setting out and painting of road-markings. Supervise slope stabilisation.

Khayelitsha Township Development. (Western Cape, South Africa)

Client: Western Cape Government | **Date:** October 1987 – August 1988

Description: Infrastructure Development

Role and Responsibilities: Senior Surveyor. Check survey road layer-works and horizontal alignment of the road works. Supervise setting out and painting of road-markings. Check survey and inspect sewer and stormwater construction.

Du Toitskloof Tunnel, (Huguenot Tunnel). (Western Cape, South Africa)

Client: National Transport Commission | **Date:** May 1986 – September 1987

Description: Road Tunnel

Role and Responsibilities: Senior Surveyor. Check-survey the contractor’s setting out before construction and survey the completed surface of the concrete paving of the road through the tunnel and the concrete paving in the portal areas, and compare the results with the design.

Survey the setting out and progress of a 50metre high rock fill and earth retaining wall, and a 70 metre deep cutting in decomposed granite and tough schist rock, plotting the results and calculating the quantities. Survey and plot cross sections of the drill and blast tunnel and compare the results with the design and contractor's profiles. Check survey installation of a large diameter steel water pipe.

Professional History

- Nov 2012 – Present | SMEC South Africa (Pty) Ltd | Technical Specialist
- Nov 2002 – Oct 2012 | VelaVKE, | Design Technologist
- Mar 1986 – Oct 2002 | VKE Engineers | Construction Surveyor
- Jan – Feb 1986 | Cape Divisional Council | Trainee Survey Technician
- Jan 1978 – Dec 1980 | Cape Divisional Council | Trainee Survey Technician

Courses & Conferences attended

2023 SANCOLD 2023 – Day
2014 Business Finances for Built Environment Professionals
2014 Road to Registration for Mentors Supervisors and HR Managers
2013 Basic Pressure Pipeline Design Course
2012 NOSA Safety Course
Global Positioning Systems Introductory Course
South African Road Federation – Storm water Drainage – 5 day Course
South African Road Federation – Contract Documentation – 3 day Course
SANRAL – Introduction to Drainage Manual - 2 day Course
AutoCAD Civil 3D – Introduction – 4 day Course

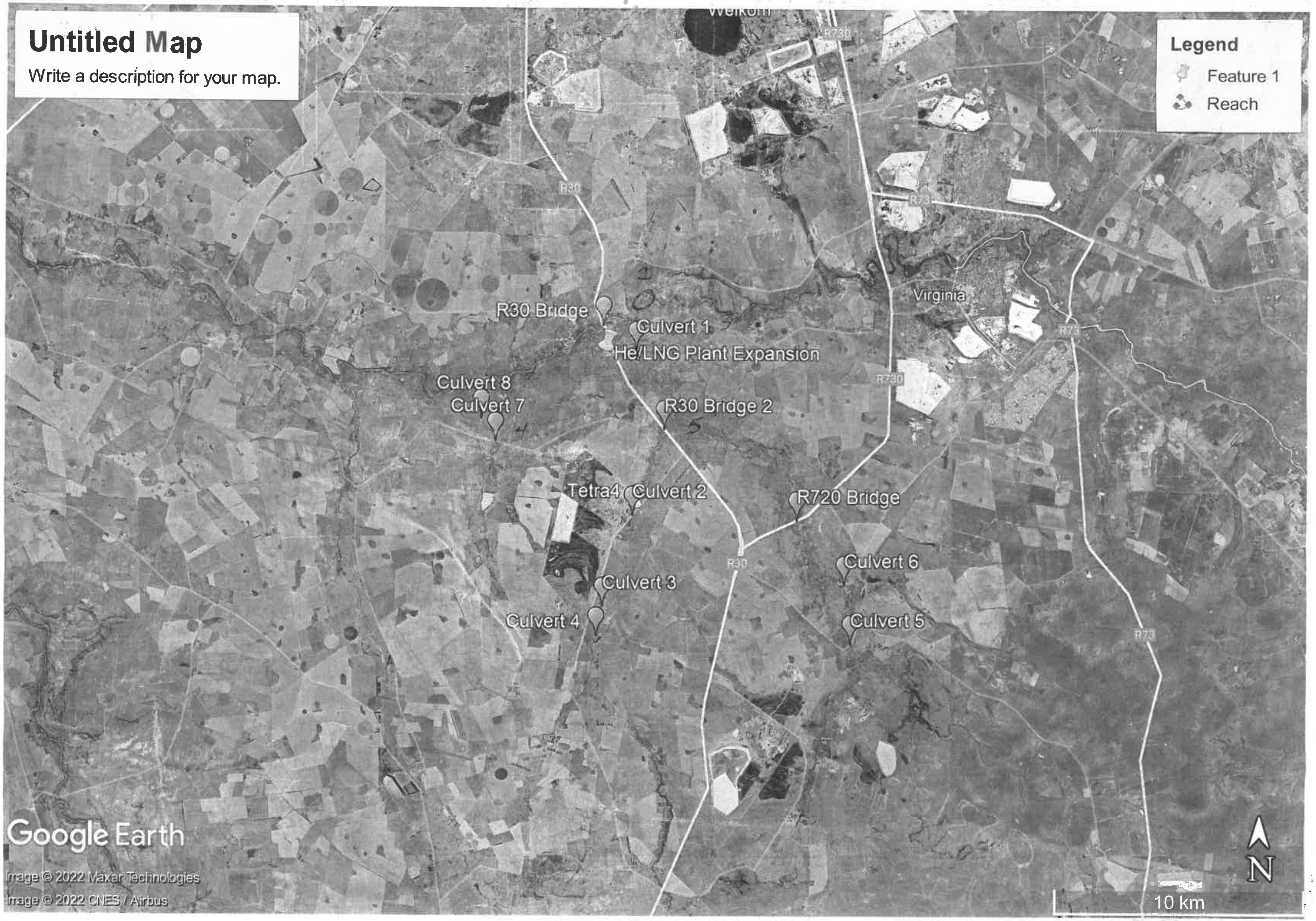
Publications & Papers presented

SANCOLD 2023 – Plugging of the Katse Diversion Tunnel No. 2 – Co-authored and present with LHDA

Language Skills

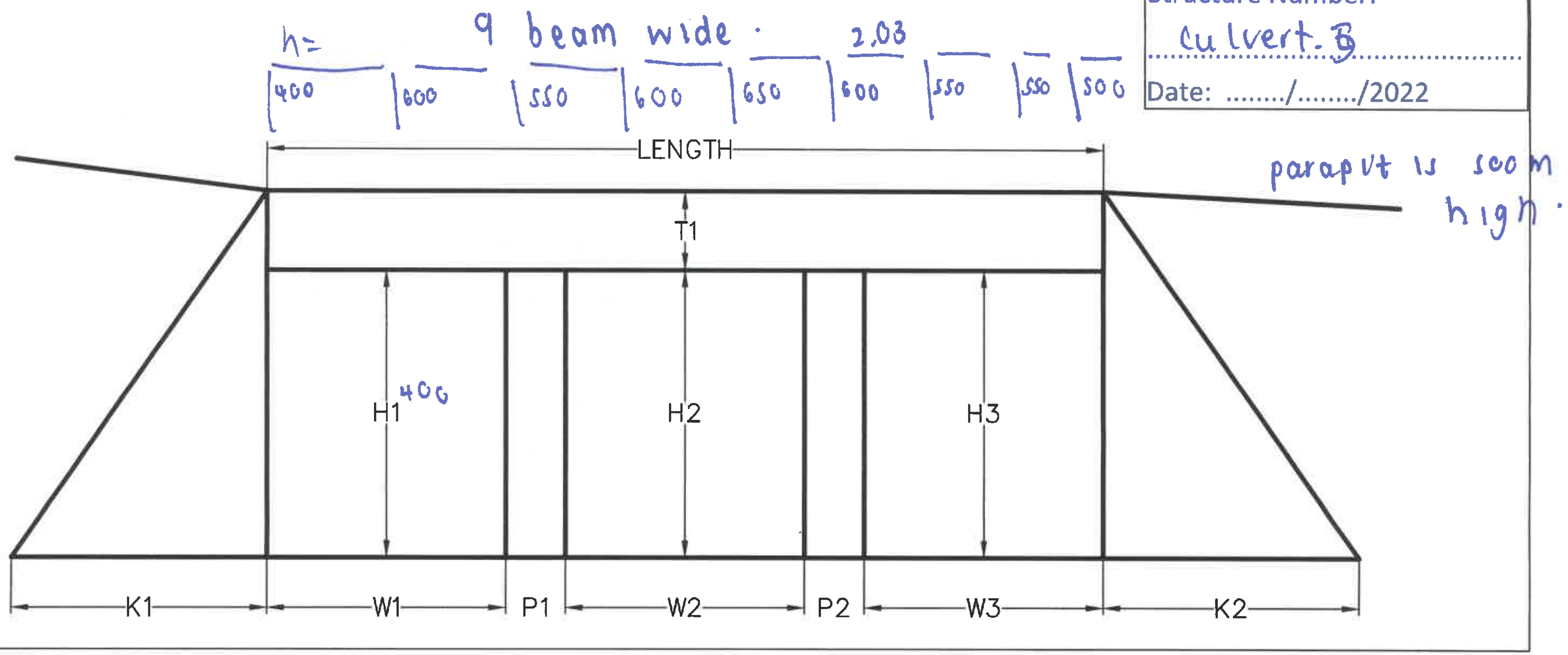
Mother Tongue:	English		
Languages	**Speak**	**Read**	**Write**
English	Excellent	Excellent	Excellent
Afrikaans	Excellent	Excellent	Excellent

Appendix F: Site Visit


Untitled Map
Write a description for your map.
Legend
Feature 1
Reach
Welkom
R730
R30
R73
Virginia
R30 Bridge
Culvert 1
He/LNG Plant Expansion
Culvert 8
Culvert 7
R30 Bridge 2
Tetra4
Culvert 2
R720 Bridge
Culvert 6
Culvert 3
Culvert 4
Culvert 5
Google Earth
Image © 2022 Maxar Technologies
Image © 2022 CNES / Airbus
10 km
N

2.03 × 0,2

~~2.03~~ 5 1,02



Structure Number: Culvert B

Date: ..../......../2022

H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 =
H2 =
H3 =
H4 =
T1 = 200mm

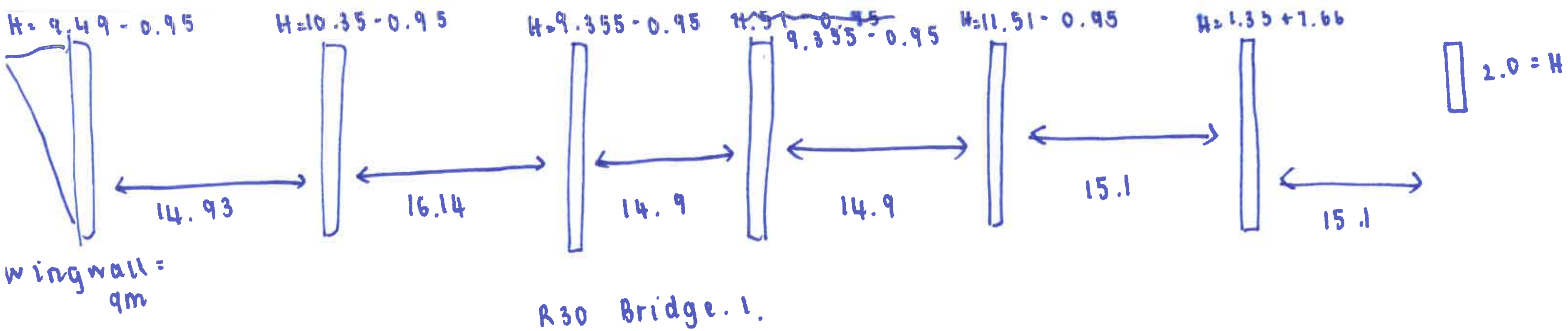
P1 =
P2 =
P3 =
P4 =
L = ~~5.47m~~ 18,45

W1 = 2,03 m
W2 = 2.03m
W3 =
W4 =
W5 =

K1u/s =
K1d/s =
K2u/s =
K1u/s =
R = 5,47

Comments:

Most of the bays/openings are overgrown.



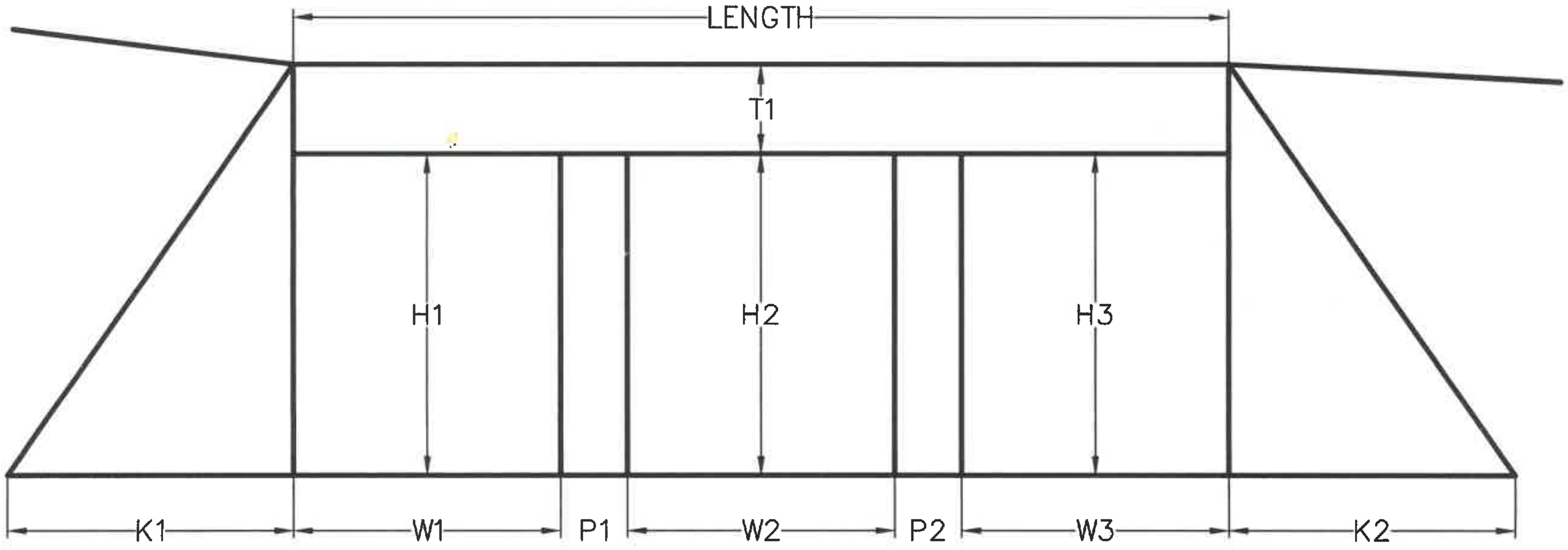
R30 Bridge. 1.

083 2764847
Mirna

450mm pipe - 300/400mm cover

Structure Number: Culvert 8.

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ____
H2 = ____
H3 = ____
H4 = ____
T1 = ____

P1 = ____
P2 = ____
P3 = ____
P4 = ____
L = ____

W1 = ____
W2 = ____
W3 = ____
W4 = ____
W5 = ____

K1u/s = ____
K1d/s = ____
K2u/s = ____
K1u/s = ____
R = ____

Comments:

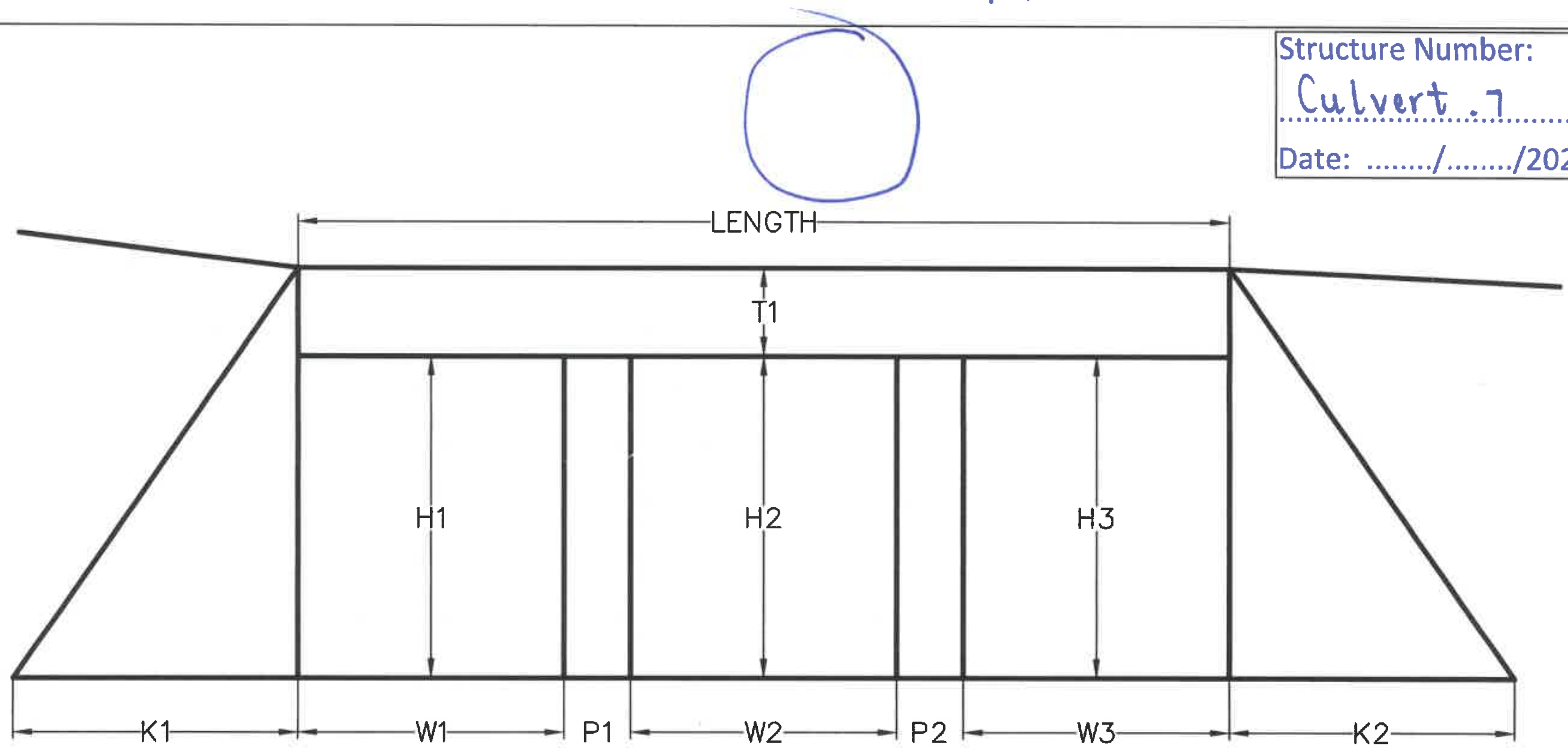
....

....

450 (model both)
~~600mm~~ pipe with a 400/500mm cover.

Structure Number: Culvert 7

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ____
H2 = ____
H3 = ____
H4 = ____
T1 = ____

P1 = ____
P2 = ____
P3 = ____
P4 = ____
L = ____

W1 = ____
W2 = ____
W3 = ____
W4 = ____
W5 = ____

K1u/s = ____
K1d/s = ____
K2u/s = ____
K1u/s = ____
R = 1.6m

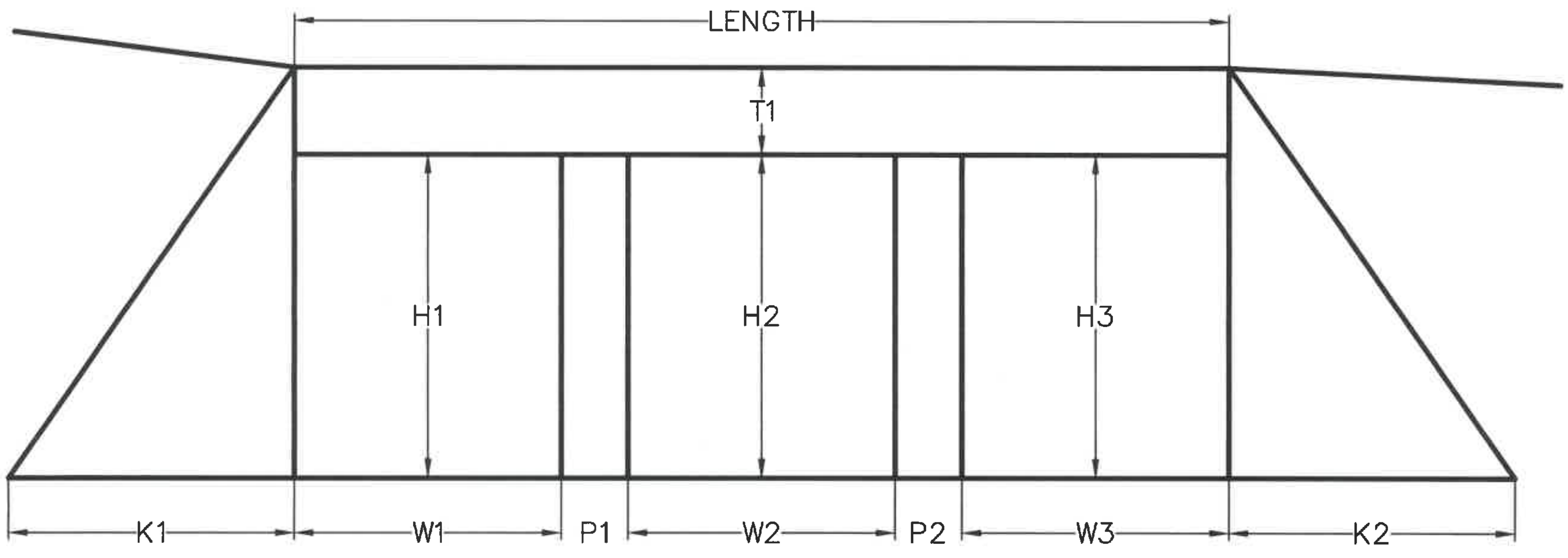
Comments:

....

....

Structure Number: culvert.14

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ____
H2 = ____
H3 = ____
H4 = ____
T1 = ____

P1 = ____
P2 = ____
P3 = ____
P4 = ____
L = ____

W1 = ____
W2 = ____
W3 = ____
W4 = ____
W5 = ____

K1u/s = ____
K1d/s = ____
K2u/s = ____
K1u/s = ____
R = ____

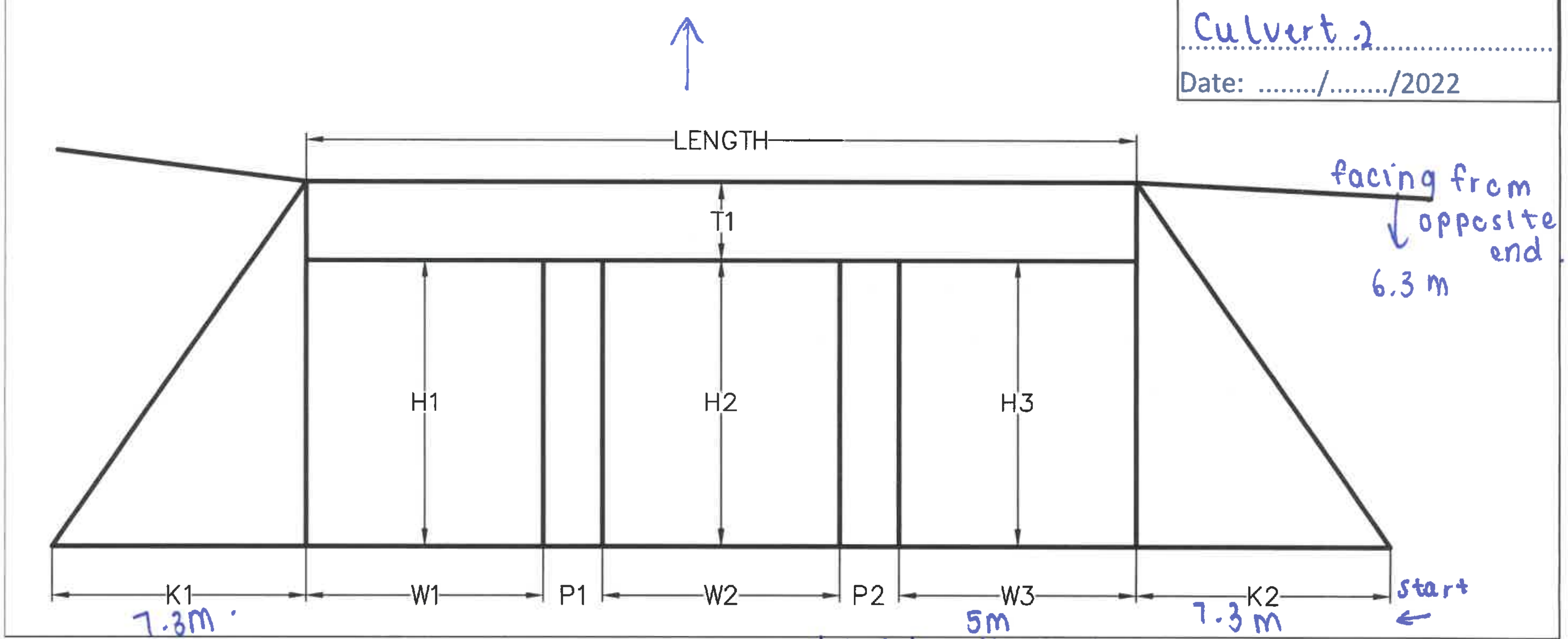
Comments:

culvert pipe abandonned / broken, ~~at~~ area has been replaced with building rubble.

Bridge No: 1695/19 81

Structure Number: Culvert 2

Date: ..../......../2022



culvert length: 27.4m

H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

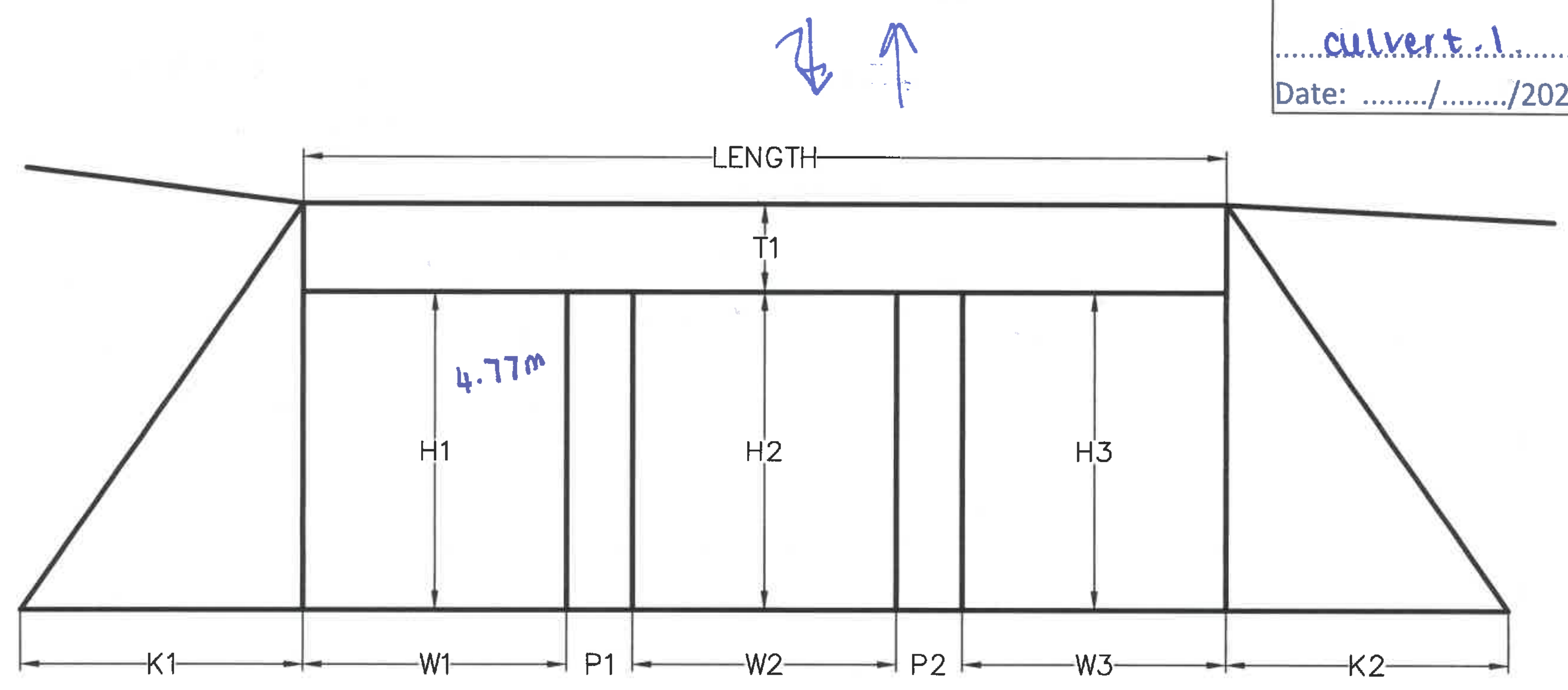
H1 = ~~3.42~~ 3.6	P1 = ~~0.5m~~ 0.475	W1 = 5.02	K1u/s =
H2 = ~~3.42~~ 2.65	P2 = 0.475	W2 = 5m	K1d/s =
H3 = 3.42	P3 = 0.475	W3 = 5 m	K2u/s =
H4 =	P4 =	W4 =	K1u/s =
T1 = 0.85m	L = 12.5m	W5 =	R =

Comments:

Deck thickness and 1m Road cover

Structure Number: culvert.1

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ____
H2 = ____
H3 = ____
H4 = ____
T1 = 1.3m

P1 = ____
P2 = ____
P3 = ____
P4 = ____
L = 42.85

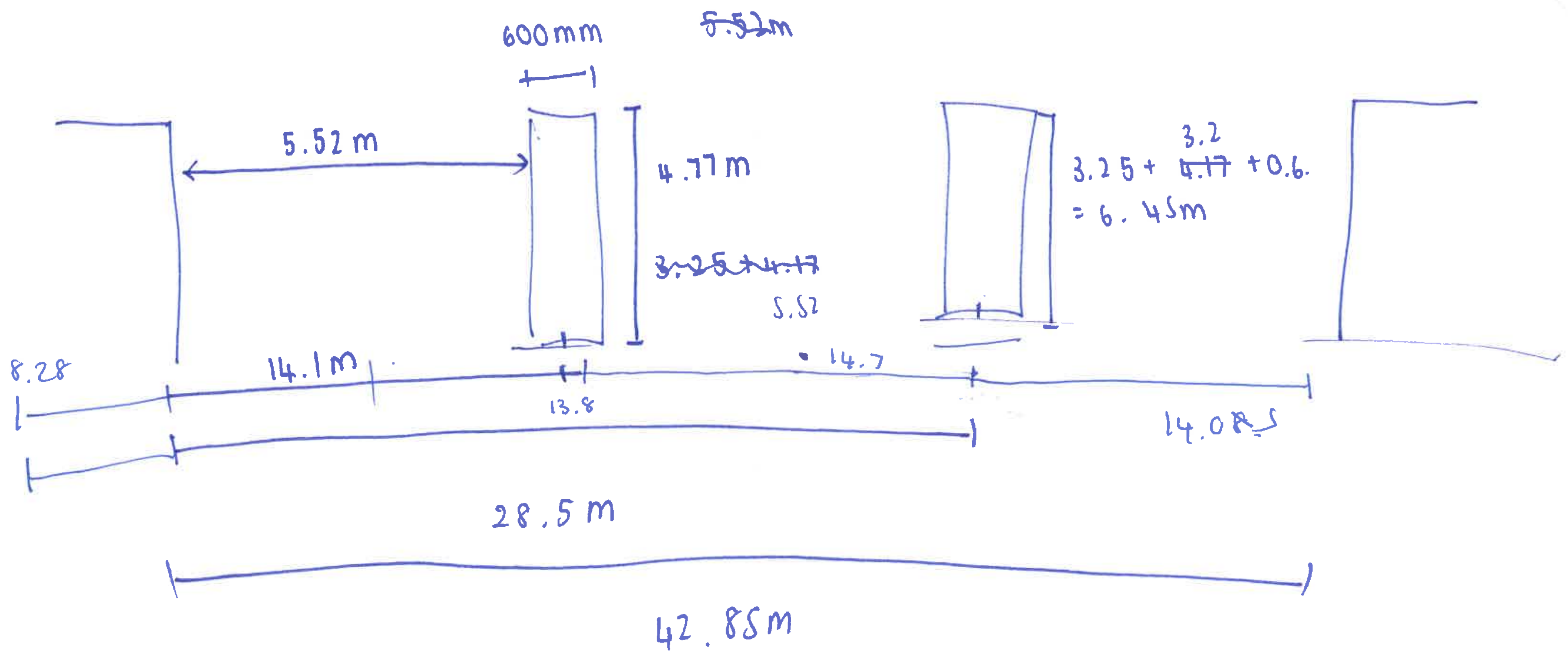
W1 = ____
W2 = ____
W3 = ____
W4 = ____
W5 = ____

K1u/s = ____
K1d/s = ____
K2u/s = ____
K1u/s = ____
R = 9.9 m

Comments:

....

....

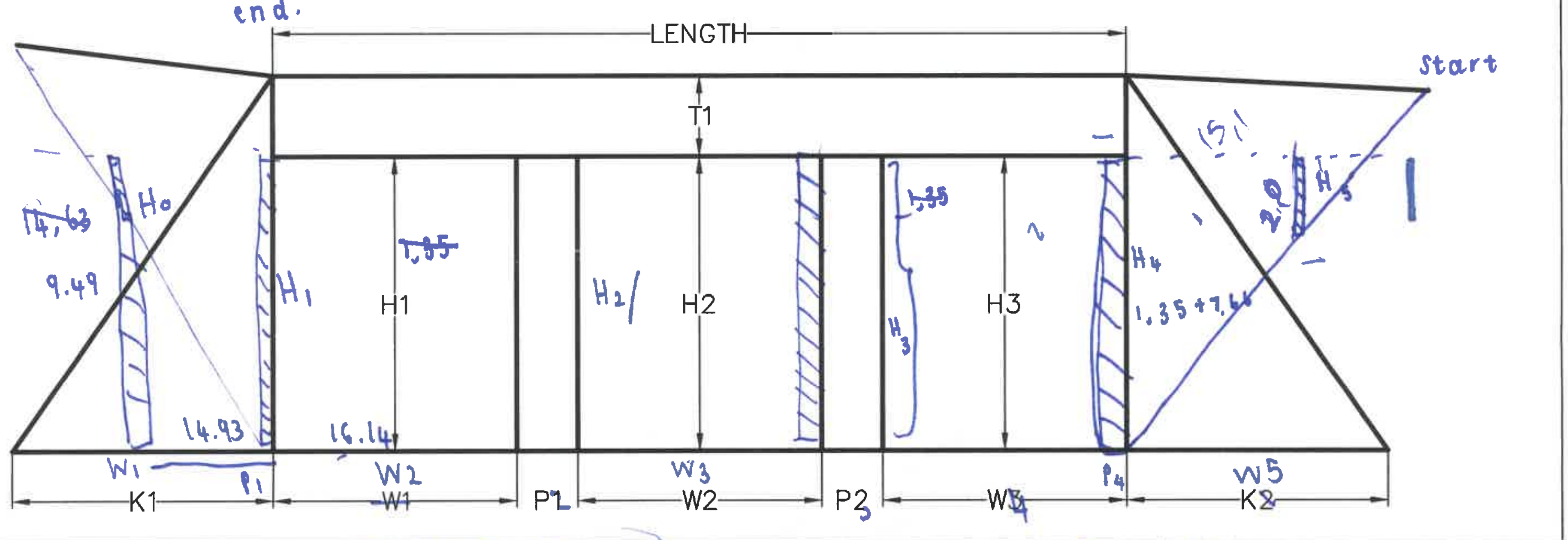


2 weirs are water affairs

(*) DWS website → look @ historical data for flows @ culvert. 1.
→ for report.

Structure Number: R30 Bridge.1

Date: ..../......../2022



width of bridge = 10.3m

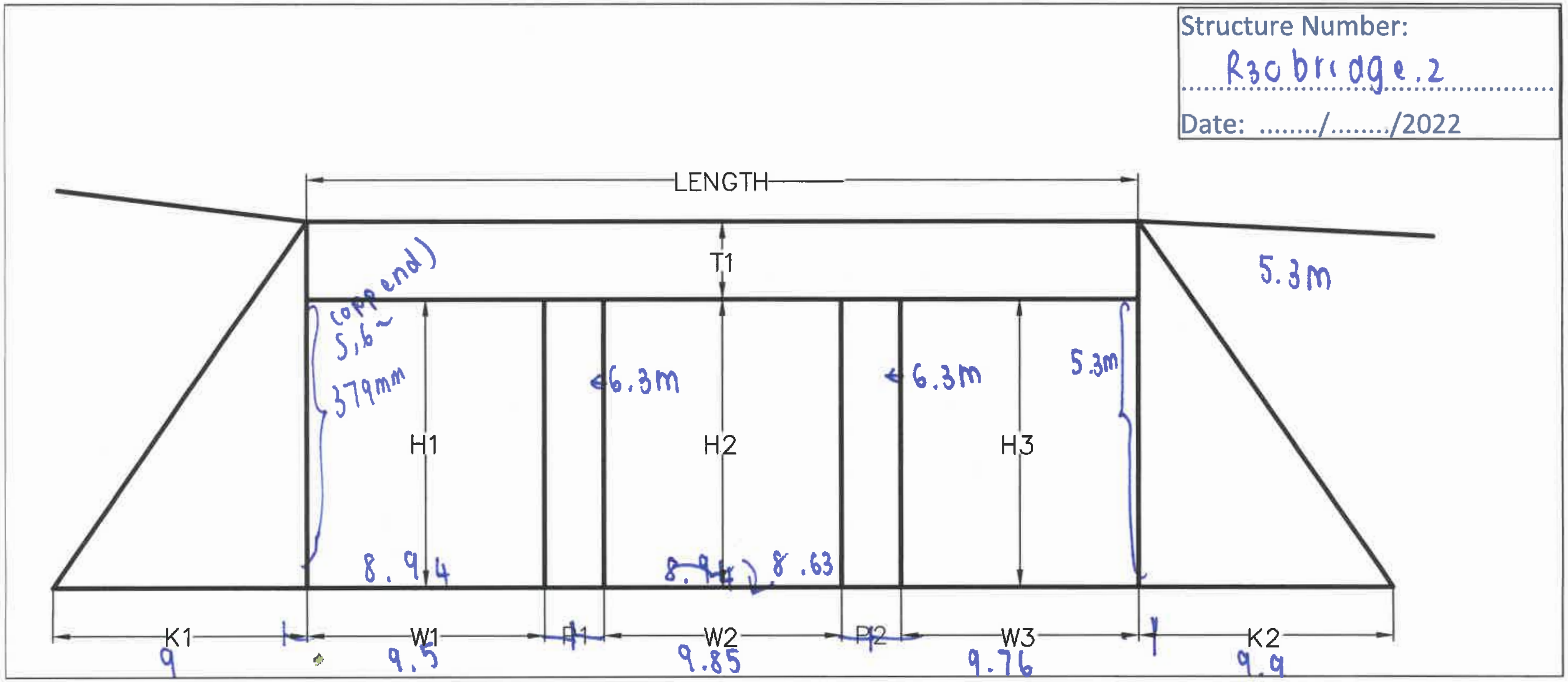
H = Height of opening	
T = Thickness of bridge deck	
P = Thickness of bridge pier	
W = Width of opening	
K = Width of bridge wing	
L = Length of bridge	
R = Road width	

H0 ~~14.63~~ 9.49-0.95

H1 = ~~1,35~~ ~~8.41~~ ~~9.07~~ 10.35-0.95	P1 =	W1 = 15,1m / 15,2	K1u/s =
H2 = 9.355 - ~~1,2~~ 0,95	P2 =	W2 =	K1d/s =
H3 = 11,51 - ~~1,2~~ 0,95	P3 = 1,5m	W3 = 14.9	K2u/s =
H4 = 1,35 + 7,88 ~~-1,2~~	P4 =	W4 = 15,1	K1u/s =
T1 = [1,4m]	L = 99 m	W5 = 15,1	R = 10.3 m

Comments:

Use T1, L, R from here. Refer to map for dimension.



H	= Height of opening
T	= Thickness of bridge deck
P	= Thickness of bridge pier
W	= Width of opening
K	= Width of bridge wing
L	= Length of bridge
R	= Road width

H1 = 6.3
H2 = 6.3
H3 = 6.3
H4 =
T1 = 650mm

P1 = 1.25m
P2 =
P3 =
P4 =
L = ~~26.9~~ 29.5

W1 =
W2 =
W3 =
W4 =
W5 =

K1u/s =
K1d/s =
K2u/s =
K1u/s =
R = 0.85

Comments:

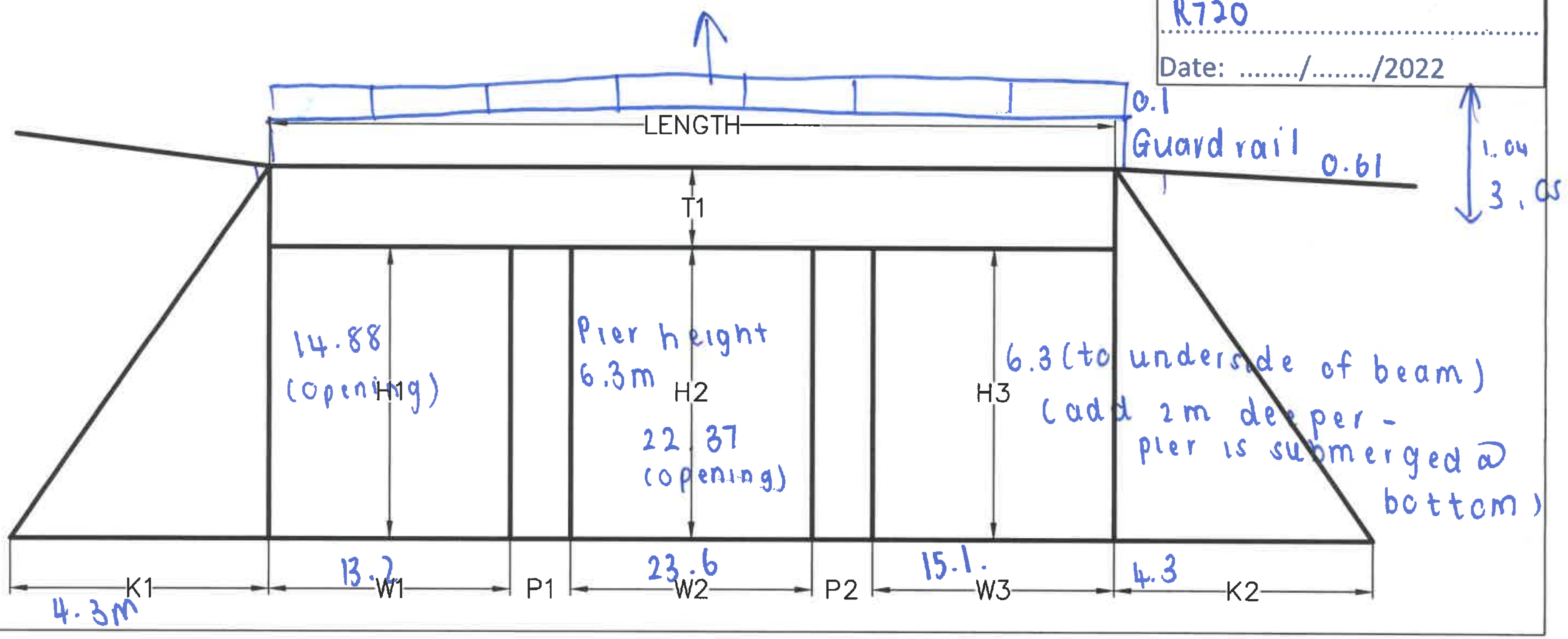
....

....

Bridge : B 875

Structure Number: R720

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

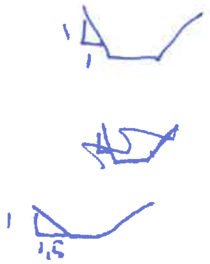
H1 =	P1 = 1.26m	W1 =	K1u/s =
H2 =	P2 = 1.26 m	W2 =	K1d/s =
H3 =	P3 =	W3 =	K2u/s =
H4 =	P4 =	W4 =	K1u/s =
T1 =	L =	W5 =	R = 13.45

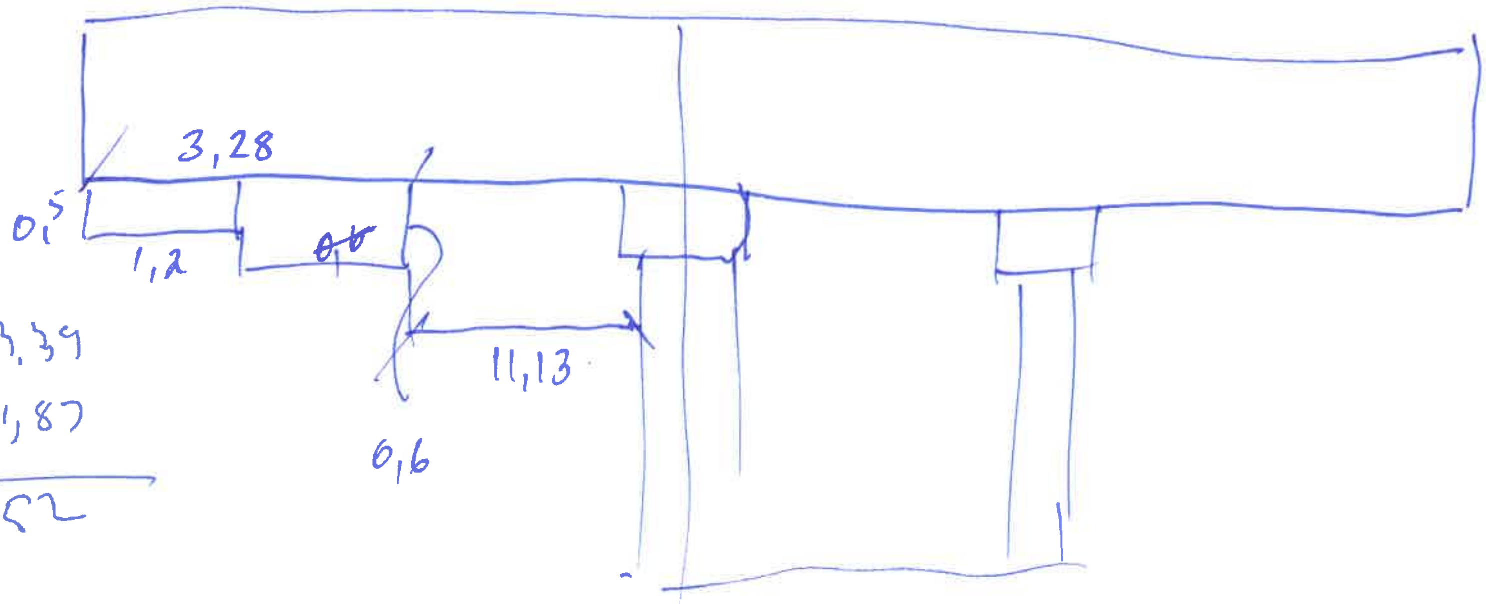
Comments:

....

....

1309.6 - 1309.8





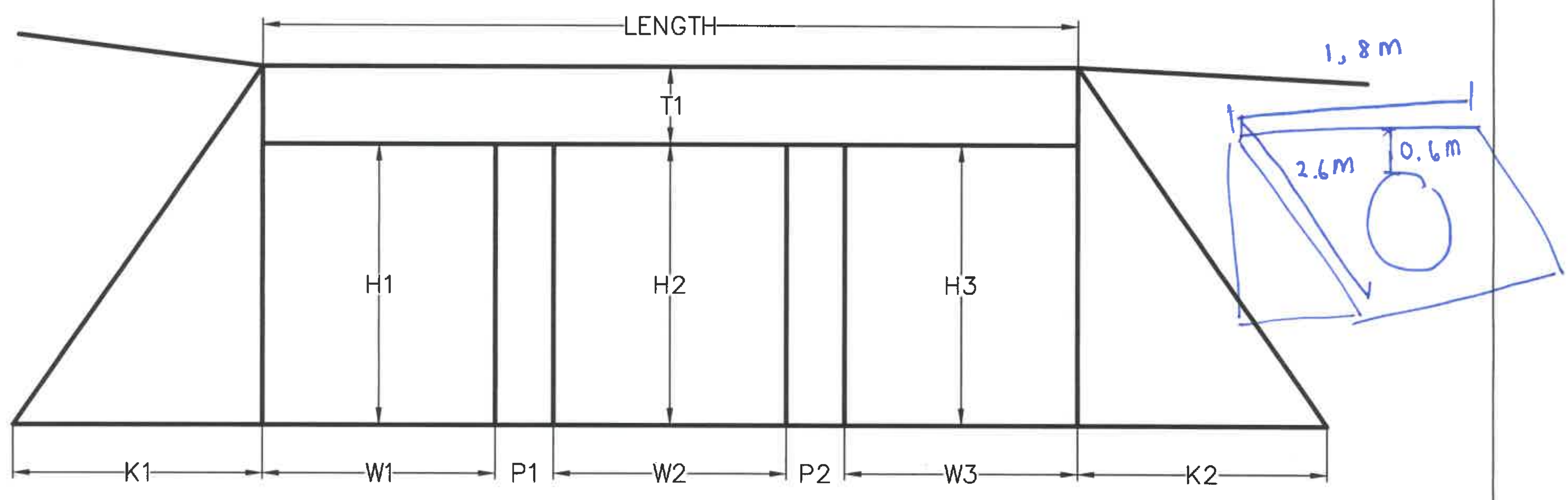
17,79	603,39
16,30	601,87
1,49	1,52

Slope is reno matteresses

Rockler culvert →
1,05m diameter (further research)

Structure Number: Culvert 6.

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ______
H2 = ______
H3 = ______
H4 = ______
T1 = ______

P1 = ______
P2 = ______
P3 = ______
P4 = ______
L = ______

W1 = ______
W2 = ______
W3 = ______
W4 = ______
W5 = ______

K1u/s = ______
K1d/s = ______
K2u/s = ______
K1u/s = ______
R = 5m

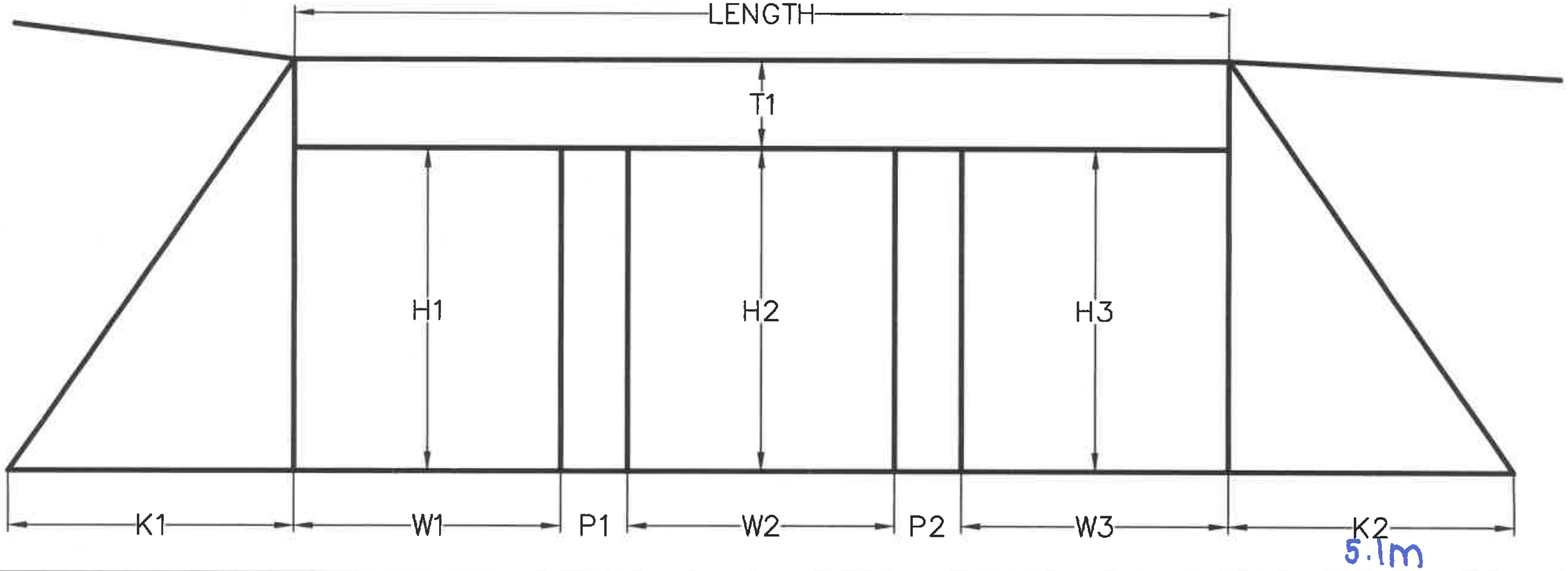
Comments:

....

....

Structure Number: culverts

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ________
H2 = ________
H3 = ________
H4 = ________
T1 = 0.45 m

P1 = ________
P2 = ________
P3 = ________
P4 = ________
L = 25.1.

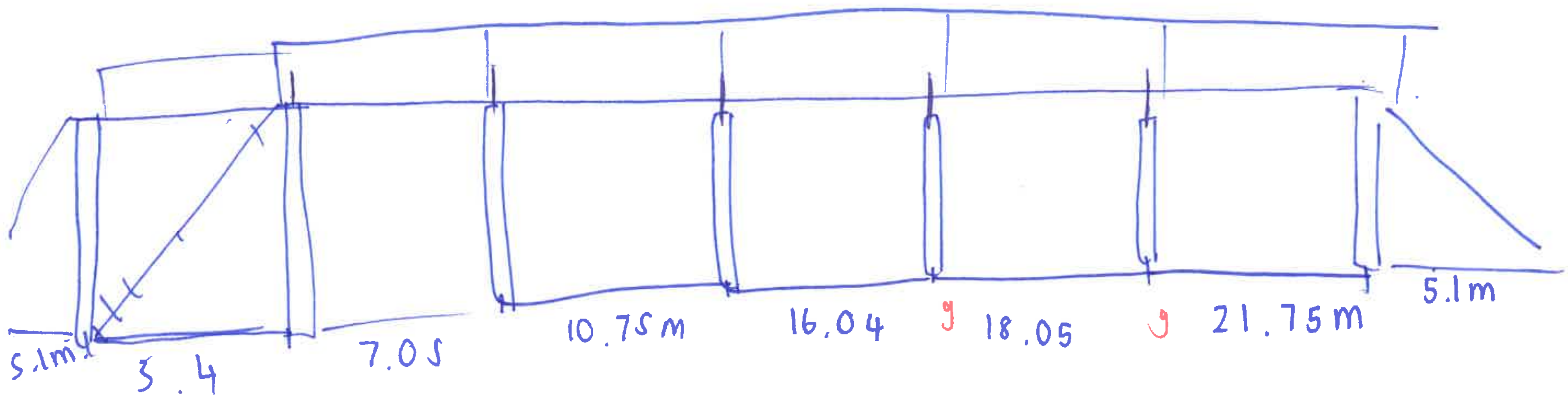
W1 = ________
W2 = ________
W3 = ________
W4 = ________
W5 = ________

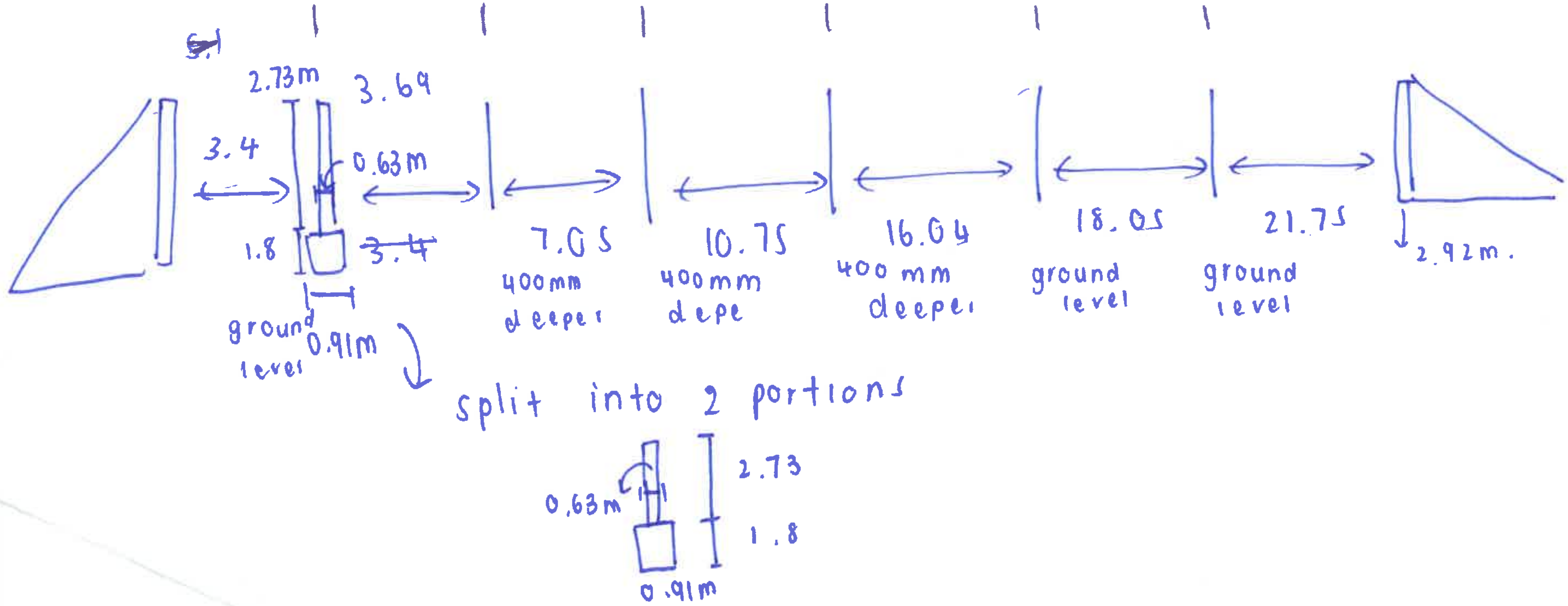
K1u/s = ________
K1d/s = ________
K2u/s = ________
K1u/s = ________
R = ________

Comments:

....

....

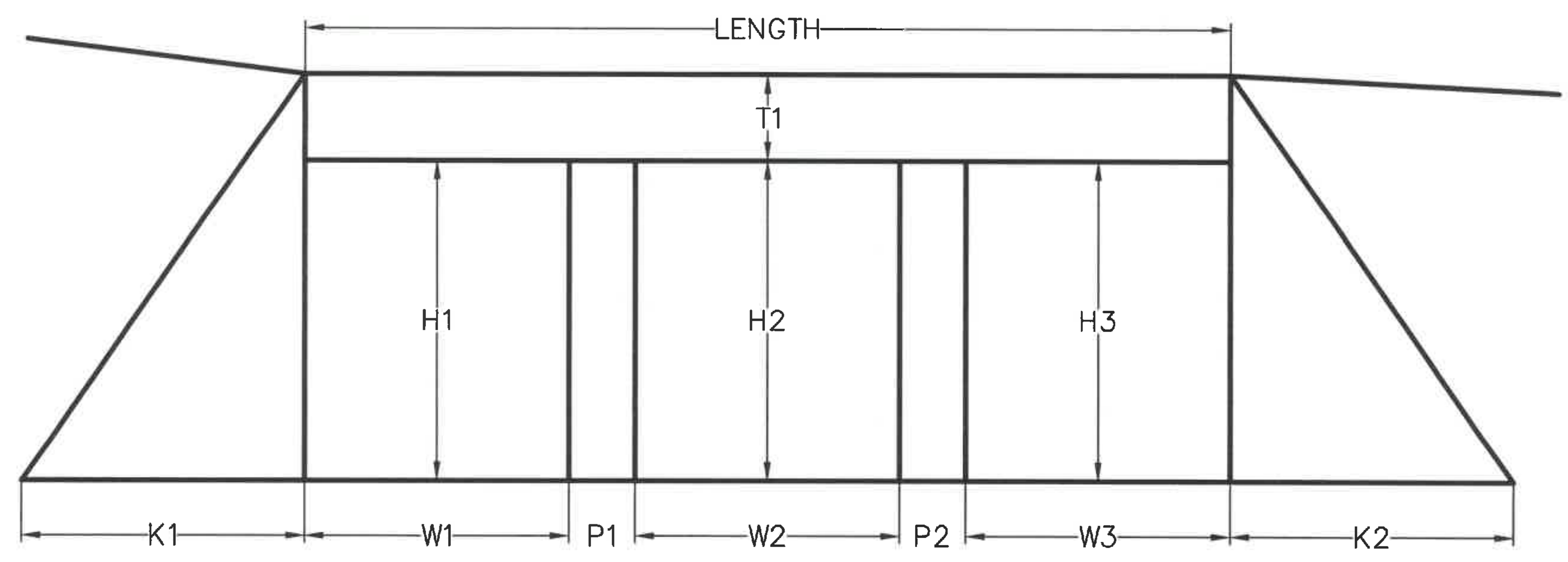

5.1m
3.4
7.05
10.75m
16.04
9
18.05
9
21.75m
5.1m


2.73m
3.69
3.4
0.63m
1.8
3.4
ground level
0.91m
7.05
400mm deeper
10.75
400mm depe
16.04
400 mm deeper
18.05
ground level
21.75
ground level
2.92m.
split into 2 portions
0.63m
2.73
1.8
0.91m

Structure Number:

....

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ______	P1 = ______	W1 = ______	K1u/s = ______
H2 = ______	P2 = ______	W2 = ______	K1d/s = ______
H3 = ______	P3 = ______	W3 = ______	K2u/s = ______
H4 = ______	P4 = ______	W4 = ______	K1u/s = ______
T1 = ______	L = ______	W5 = ______	R = ______

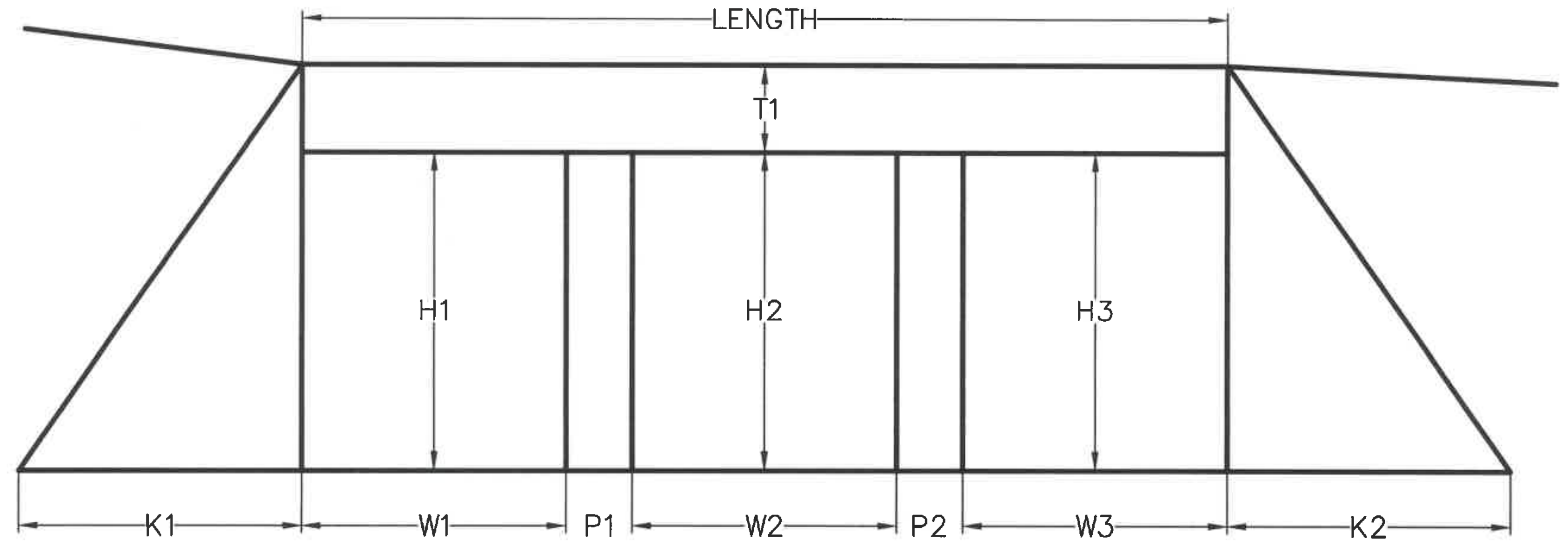
Comments:

....

....

Structure Number: ....

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ______	P1 = ______	W1 = ______	K1u/s = ______
H2 = ______	P2 = ______	W2 = ______	K1d/s = ______
H3 = ______	P3 = ______	W3 = ______	K2u/s = ______
H4 = ______	P4 = ______	W4 = ______	K1u/s = ______
T1 = ______	L = ______	W5 = ______	R = ______

Comments:

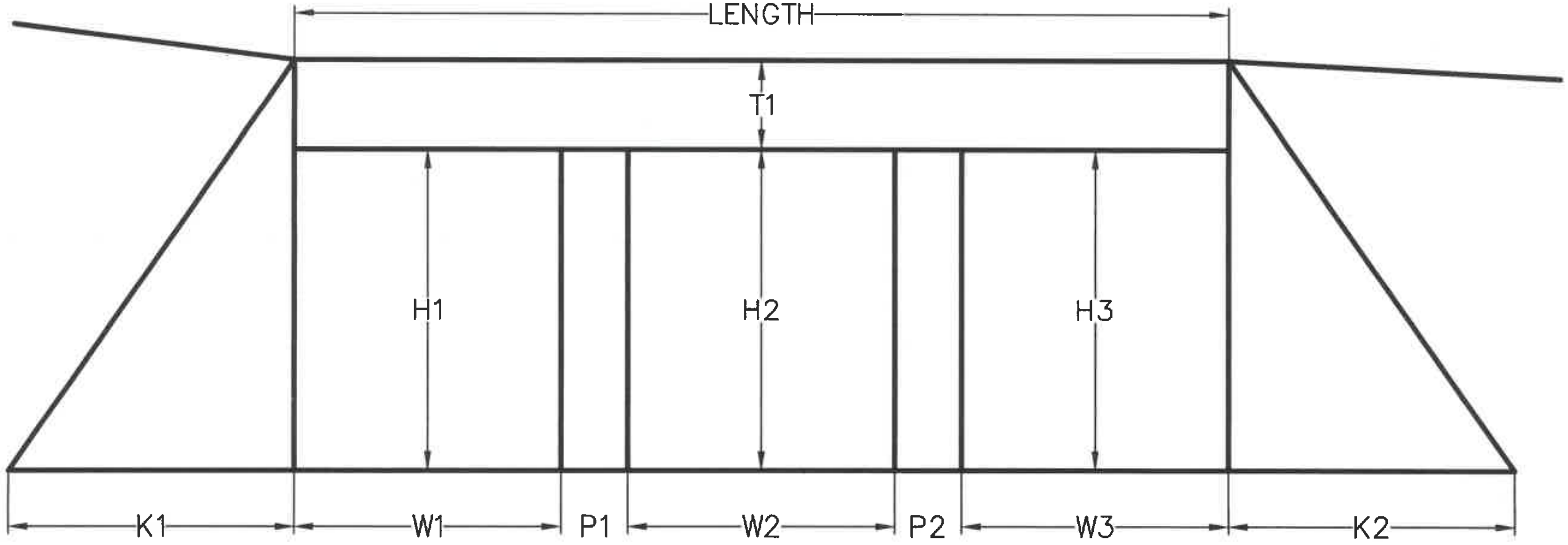
....

....

Structure Number:

....

Date: ..../......../2022



H = Height of opening
T = Thickness of bridge deck
P = Thickness of bridge pier
W = Width of opening
K = Width of bridge wing
L = Length of bridge
R = Road width

H1 = ____________
H2 = ____________
H3 = ____________
H4 = ____________
T1 = ____________

P1 = ____________
P2 = ____________
P3 = ____________
P4 = ____________
L = ____________

W1 = ____________
W2 = ____________
W3 = ____________
W4 = ____________
W5 = ____________

K1u/s = ____________
K1d/s = ____________
K2u/s = ____________
K1u/s = ____________
R = ____________

Comments:

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Structure Number:

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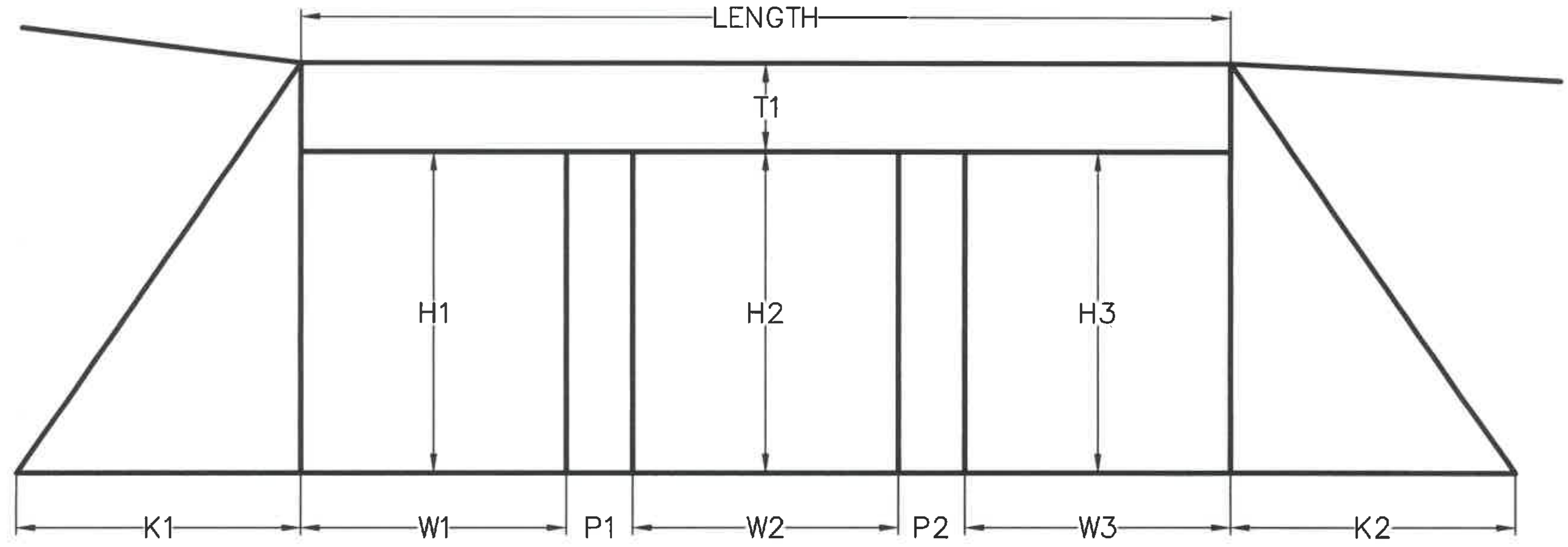
Date: ..../......../2022



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P3 = ____________
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W2 = ____________
W3 = ____________
W4 = ____________
W5 = ____________

K1u/s = ____________
K1d/s = ____________
K2u/s = ____________
K1u/s = ____________
R = ____________

Comments:

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